DEPARTMENT OF THE AIR FORCE HEADQUARTERS 377TH AIR BASE WING (AFGSC)



Mr. L. Wayne Bitner Chief, Environmental Restoration 2000 Wyoming Blvd SE Kirtland AFB NM 87117-5600

DEC 21 2015

ENTERED

Ms. Michelle Hunter Ground Water Quality Bureau New Mexico Environment Department 1190 St Francis Drive Santa Fe, New Mexico 87502

Subject: Request for Temporary Permission to Discharge for Pilot Test KAFB-7 Gravity Injection, Bulk Fuels Facility, Kirtland Air Force Base, New Mexico

Dear Ms. Hunter

A Class V underground injection control (UIC) discharge permit application (UIC application; DP-1839) was submitted to the New Mexico Environment Department (NMED) Ground Water Quality Bureau (GWQB) on December 4, 2015. This UIC permit application describes a system that will consist of up to five injection wells to support the ethylene dibromide (EDB) plume Interim Measure (IM) Kirtland Air Force Base (KAFB) is implementing to address the historical fuel leak from the former Bulk Fuel Facility (BFF). The application was determined to be administratively complete by the GWQB letter dated December 17, 2015.

This letter requests that the GWQB issue a temporary permission (TP) pursuant to the UIC application to allow KAFB to implement an injection well pilot test. This test will be performed in production well KAFB-7, which is being retrofitted as an injection well. The objective of this pilot test is twofold: to evaluate the feasibility of using KAFB-7 as an injection well and to have a winter 2016 water disposition option for the treated groundwater from the full-scale groundwater treatment system (GWTS).

The scope of work for this pilot test is described in the following documents:

- The September 18, 2015 Rapid Response Action to Notice of Violation Groundwater Disposition Work Plan;
- The October 30, 2015 Groundwater Disposition Letter Work Plan Addendum #1; and
- The November 9, 2015 Groundwater Disposition Letter Work Plan Addendum #2.

Background

Some of scope described in these documents has already been performed so that the pilot test may begin immediately upon receipt of the TP. As detailed in the attached "Well KAFB-7 Pumping/Recovery Test and Well Rehabilitation Report":

- A pumping/recovery test was performed in October 2015 to ensure that KAFB-7 is capable of accepting the anticipated maximum 400 gallons per minute (gpm) of treated groundwater;
- A pre-rehabilitation well video survey was conducted on October 26, 2015;
- Well rehabilitation activities were performed from November 5 through 12, 2015 to remove debris and screen incrustations;
- A downhole camera was used on November 23, 2015 to obtain a post-rehabilitation well video



Survey (DVDs of the video footage were provided to the GWQB); and

 A V-Smart Injection Valve (downhole flow control valve) was installed in KAFB-7 on December 1 and 2, 2015 (the top of the valve placed at approximately 560 feet).

The "Well KAFB-7 Pumping/Recovery Test and Well Rehabilitation Report" concludes that Well KAFB-7 is capable of accepting the anticipated maximum 400 gallons per minute (gpm) of treated groundwater with only a 5-foot rise in water table. Additionally, water levels will be monitored with transducers near (KAFB-10523, KAFB-10524, KAFB-10507, and KAFB-10508) and in Well KAFB-7. The water level monitoring along with United States Geological Survey gravity survey at Well KAFB-7 will be used to evaluate water entering the regional aquifer and will be used to monitor any potential impacts of injection on Well KAFB-7.

Groundwater samples were collected from KAFB-7 and treated effluent from the GWTS to determine how injection may influence geochemistry in the regional aquifer using PHREEQC geochemical modeling. Summary results reported in email from Dr. Patrick Longmire dated December 11, 2015, indicates that "clogging of the KAFB-7 well screen is not likely, based on the close chemical similarities of treated effluent and groundwater". A final report will be prepared by Dr. Patrick Longmire detailing model construction and results of the simulations and will be submitted January 31, 2016.

Temporary Permission Request

KAFB is requesting a maximum allowable discharge rate of 500 gpm, which will accommodate any fluctuation in the volume of treated groundwater from the full-scale GWTS. As detailed in the UIC application the effluent from the full-scale GWTS will not exceed the lowest of the applicable federal maximum contaminant limit (MCL) or human health standard in 20.6.2.3103(A) NMAC.

We appreciate your attention to this matter. Please contact me at 505.853.3484 or at ludie.bitner@us.af.mil or Mr. Scott C. Clark at 505.846.9017 or at scott.clark@us.af.mil if you have any questions.

Sincerely,

L. Wayne Bitner Chief, Environmental Restoration

Attachment: Well KAFB-7 Pumping/Recovery Test and Well Rehabilitation Report

cc:

NMED-EHD (Roberts) NMED (McQuillan, Longmire, Agnew) NMED-HWB (Kieling, Cobrain) NMED-GWQB (Huddleson, Pullen) NMED-PSTB (Reuter) NMED-OGC (Kendall) SAF-IEE (Lynnes) AFGSC 377th ABW (Col Froehlich) U.S.EPA Region 6 (King, Ellinger) AFCEC-CZRX (Bodour) AFCEC-CZOW (Bitner, Branson, Clark) USACE-ABQ District Office (Simpler, Phaneuf) Public Info Repository (Central New Mexico Community College), Administrative Record/Information Repository (AR/IR), and File

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ATTACHMENT

Prepared by CB&I Federal Services LLC 2440 Louisiana Blvd. NE, Suite 300 Albuquerque, NM 87110 Tel: +1 505 262 8800 Fax: +1 505 262 8855 www.CBI.com

December 7, 2015

Subject: Draft Well KAFB-7 Pumping/Recovery Test and Well Rehabilitation Report

Executive Summary

This Letter Report describes the pumping and recovery test conducted at Kirtland Air Force Base (KAFB) production well KAFB-7 in October 2015 as well as work performed in accordance with Groundwater Disposition Letter Work Plan Addendum #1 dated October 30, 2015 (USACE, 2015a) and Addendum #2 dated November 9, 2015 (USACE, 2015b). The pumping and recovery test was conducted prior to well rehabilitation and retrofitting of KAFB-7 for use as an injection well. This well will be used to dispose of treated groundwater from the pump-and-treat interim measure designed to collapse the solid waste management unit (SWMU) ST-106/SS-111 dissolved ethylene dibromide (EDB) groundwater plume. The results of this test show that KAFB-7 is capable of accepting the anticipated maximum 400 gallons per minute (gpm) of treated groundwater.

KAFB-7 was pumped for 24 hours and allowed to recover for 72 hours. Data from the pumping well and observation wells were corrected for non-pumping stresses, and there was measurable drawdown in two observation wells, KAFB-0508 and KAFB-0523, which are located 194 and 860 feet respectively from KAFB-7. After 24 hours of pumping, the well efficiency was estimated to be 54 percent (%). Based on the data analyses, the aquifer transmissivity was 34,000 square feet (feet²) per day, hydraulic conductivity was 90 feet per day, the specific yield was 0.027, and the specific storage was 7.6×10^{-6} per foot. These results were used to calculate that, at a maximum injection rate of 400 gpm, the water level adjacent to KAFB-7 would rise approximately 5 feet. Since there is 43 feet of screen above the water table, an anticipated rise of only 5 feet indicates that KAFB-7 is suitable for use as an injection well.

KAFB-7 was purged, sampled, and rehabilitated to support injection. The KAFB-7 rehabilitation and valve installation summary of activities conducted are described below.

Pumping and Recovery Test Procedure

KAFB-7 was turned off 4 days prior to the start of the test. Pressure transducers were installed in four observation wells (Table 1 and Figure 1). A pressure transducer was attached to the air line feeding into KAFB-7 to monitor water levels in accordance with the method described on pages 550 to 552 of *Groundwater and Wells* (Driscoll, 1986).

A 24-hour pumping test began at noon on October 6, 2015. At the end of the 24-hour pumping period, a sample was collected for total and dissolved metals by U.S. Environmental Protection Agency (EPA) Method 6020, total and dissolved silicon by EPA Method 6010, anions by EPA Method 300, total and dissolved alkalinity by Standard Method (SM) 2320B, total dissolved solids by SM2540C, total and dissolved organic carbon by SM5310B, and total Kjeldahl nitrogen by SM4500. Following sampling, the pump was shut off at noon on October 7, 2015, and the aquifer was allowed to recover for a 72-hour period while the pressure transducers continued to record water-level changes.

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Data and Analysis

Sampling

The preliminary sampling results are provided in Table 2. None of the analyte concentrations exceeded their respective regulatory limits.

Data Corrections

The determine the response of observation wells during pumping and recovery, water levels were corrected for non-pumping stresses, including barometric fluctuations and regional water-level changes. Well KAFB-0524 was located approximately 2570 feet from KAFB-7, which put it outside of the expected zone of influence from pumping at KAFB-7. Therefore, the displacement observed at KAFB-0524 was responding only to non-pumping stresses during testing. As a result, the water-level displacement in KAFB-0524 was subtracted from the displacement observed in each of the other test wells to correct the data at those wells for non-pumping stresses. The corrected water levels for the duration of pumping and recovery are presented on Figure 2 for observation wells and on Figure 3 for KAFB-7. Two of the observation wells, KAFB-0508 and KAFB-0523, had a response to pumping of KAFB-7 sufficient for the determination of aquifer characteristics (Figure 2).

The water level in KAFB-0507 responded to an additional stress, most likely the pumping at another production well (Figure 2); the same response was observed in the recovery water levels in KAFB-7 (Figure 3). Both of these wells had screen intervals in a deeper part of the aquifer than the remaining test wells, which may explain why the other wells did not respond to the same stress. This signature was removed from the KAFB-7 data by subtracting the corrected displacement observed in KAFB-0507; the results are presented on Figure 3.

As shown on Figure 4, there was an initial water-level drop of approximately 8.8 feet observed in KAFB-7 when the pump first turned on and the drop pipe filled with water with little back-pressure. Once the pipe was filled, by 4 minutes into the test, the additional pressure in the pipeline caused the pumping rate to decrease, and the water level recovered to a displacement of approximately 4.4 feet below the prepumping level. After this, the water level steadily declined for the duration of pumping. Likewise, there was an initial rise in water level of approximately 8.4 feet when the pump was shut off, and the water from the drop pipe drained into the well. By 6 minutes into the recovery period, the water level declined to a displacement of approximately 5.4 feet above the water levels at the end of pumping, approximately 0.5 foot below the pre-pumping level. After this, the water level steadily rose until it stabilized at the pre-pumping level, approximately 900 minutes (15 hours) after the pump was shut off. These initial pumping and recovery pump-related pulse data were removed from both the pumping and recovery data sets prior to analysis.

Assumptions

The following assumptions were made prior to analysis, and are based on data obtained during testing and from KAFB-7 documentation:

- 1. To calculate aquifer characteristics, both pumping and recovery data were analyzed.
- 2. The aquifer is characterized as unconfined; therefore, analysis methods applicable to unconfined conditions were used.
- 3. For the data analysis, the pumping well is characterized as fully penetrating in the aquifer. The liner installed in 1979 has mill slots from 578 feet down to 1,010 feet—the original bottom of the well. The top of the original louvered screen, the top of which is 43 feet above the current water level at 486

feet, is assumed to be in hydraulic communication with the aquifer and the slotted liner. The bottom 60 feet of the well is filled with material and heavy incrustation has covered the majority of slots below a depth of 851 feet. Therefore, for calculating hydraulic conductivity and specific storage, an aquifer thickness of 365 feet of water is used (851'-486' = 365'). If the full aquifer thickness of 488 feet is used for calculating these two parameters, the results will be reduced by 25% (100*(1-(365'/488')) = 25%).

Aquifer Characteristics Analysis Method

The aquifer testing software AQTESOLV[®] (Duffield, 2007) was used to conduct the analysis of aquifer characteristics. The Moench (1997) solution for unsteady flow to a fully or partially penetrating finite diameter well with well-bore storage and skin effect in a homogeneous, anisotropic unconfined aquifer with delayed gravity response was selected as the analytical solution to determine aquifer properties. This method generates values for transmissivity (T), storage coefficient (S), hydraulic conductivity (K), and specific yield (Sy). The Moench solution also allows for the determination of values for the ratio of horizontal to vertical hydraulic conductivity times radial distance squared and divided by aquifer thickness squared ($\beta = K_z t^2/K_r b^2$), well-bore skin effect (Sw), nominal casing radius (r(c)), effective well radius (r(w)), and an empirical constant for delayed drainage from the water table (α_1).

The method developed by Agarwal (1980) was used to apply the Moench (1997) analytical solution to the recovery data. In this method, equivalent time and recovery drawdown for recovery data are calculated using the following formulas:

$$t_{equiv} = \frac{t_p - t'}{t_p + t'}$$
$$s_r = s_n - s'$$

where:

t_{equiv} is the Agarwal equivalent time

t' is time since pumping stopped

 t_{p} is the total time of pumping

sr is recovery drawdown

 s_p is drawdown in well at time t_p ,

s' is residual drawdown in the well after pumping stopped

Results

At 24 hours of pumping at an average discharge rate of 740 gpm, the drawdown in KAFB-7 was 5.89 feet, resulting in an estimated specific capacity of 120 gpm per foot. With extended pumping until drawdown stabilizes, it is expected that the specific capacity estimate would decrease, possibly by as much as 50%, or 60 gpm per foot. This is consistent with the original specific capacity of 64 gpm per foot measured upon well installation. Following the KAFB-7 well rehabilitation in 2002, a specific capacity test indicate 16 gpm per foot, which is significantly lower than either the initial or 2015 specific capacity estimates.

At KAFB-7, a well efficiency of 54% was calculated after 24 hours of pumping. To determine well efficiency, the drawdown at observation wells KAFB-0508 and KAFB-0523 was plotted versus the distance from the pumping well on a semi-log plot (Figure 5). A straight line was projected through these points onto the KAFB-7 casing radius (1 foot). The point where the projected line met the radius was the

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expected drawdown in the pumping well for a 100% efficient well. The well efficiency is the expected drawdown divided by the observed drawdown in the pumping well.

Table 3 summarizes the results of the Moench (1997) analysis on recovery data for the pumping well and observation wells, and the results for each well are provided in Attachment 1. Using the geometric mean of analysis results, the aquifer transmissivity was 34,000 feet² per day, hydraulic conductivity was 90 feet per day, the specific yield was 0.027, and the specific storage was 7.6×10^{-6} per foot.

To determine the expected rise in water level in the vicinity of KAFB-7 based on the maximum -anticipated injection rate, the following equation for an injection well penetrating an unconfined aquifer at -steady state was used (Driscoll, 1986):

$$Q_r = \frac{K(h_w^2 - H_0^2)}{1055\log((r_0/r_w))}$$

rearranged to:

$$h_{w} = \left(\frac{Q_{r} \times 1055\log[r_{o}/r_{w}]}{K} + {H_{0}}^{2}\right)^{1/2}$$

where:

 $h_{\rm w}$ is the head above the bottom of the aquifer while recharging (in feet)

Q_r is the injection rate (gpm)

K is the hydraulic conductivity (gallons per day per square foot [gpd per foot²])

H₀ is the static head above the bottom of the aquifer (feet, equal to the aquifer thickness)

 r_0 is the radius of influence (feet)

 r_w is the injection well radius (feet)

The anticipated rise in water level would therefore be equal to $h_w - H_0$.

The following conservative values were assumed for the input parameters:

- $Q_r = 400$ gpm. This is the maximum anticipated injection rate.
- K = 340 gpd per foot². This converts to 45 feet per day, which is half of the calculated hydraulic conductivity of 90 feet per day (670 gpd per foot²) to account for the estimated well efficiency of 54%.
- $H_0 = 365$ feet. This is the aquifer thickness used for data analysis.
- r₀ = 1,300 feet. During the 24-hour pumping period, drawdown was observed in KAFB-0523, 860 feet from KAFB-7, and not in the next closest well, KAFB-0507, at a distance of 1,340 feet from KAFB-7. The value of 1,300 feet assumes that KAFB-0507 is only 40 feet beyond the radius of influence, and is consistent with the distance drawdown plot on Figure 5.
- $r_w = 1$ foot. This is the radius of KAFB-7.

Using these values, h_w was calculated as 370 feet, which is 5 feet higher than the H₀ value of 365 feet.

Pumping and Recovery Test Conclusions

Based on the data analysis presented here, there is an expected rise in water level of 5 feet at KAFB-7 at a maximum anticipated injection rate of 400 gpm. Because there is 43 feet of louvered screen in the original casing above the water table, an anticipated rise of only 5 feet indicates that KAFB-7 is capable of accepting the treated groundwater from the pump-and-treat interim measure designed to collapse the SWMU ST-106/SS-111 dissolved EDB groundwater plume.

Well Rehabilitation and Valve Installation Summary

The following activities were conducted at well KAFB-7:

- On November 4, 2015, slightly more than three casing volumes (approximately 9,118 gallons) were
 purged from KAFB-7 to remove flocculant. Groundwater was then sampled for primary drinking
 water standards for metals (EPA Method 200.8 for 18 metals), nitrate/nitrite (EPA Method 300.0),
 total Kjehldahl nitrogen (TKN) (EPA Method 351.2), total nitrogen (by calculation), volatile organic
 compounds (EPA Method 524.2), and ethylene dibromide (EDB) (EPA Method 504.1). None of the
 results were greater than the drinking water regulatory standards. The samples were analyzed in
 accordance with the Groundwater Disposition Letter Work Plan Addendum #1 dated October 30,
 2015 (USACE, 2015a) and NMED's response letter dated November 12, 2015.
- On November 5, 2015, plastic strip debris was successfully removed from KAFB-7. This debris had been identified during the initial pre-rehabilitation well video survey conducted on October 26, 2015.
- On November 11, 2015, a wireline nylon Cotey casing brush, built to fit tightly inside the well, was used to brush and swab the length of the well. Additional effort was focused on brushing and swabbing from approximately 580 feet to 700 feet where there was less incrustation visible in the pre-rehabilitation well video.
- On November 12, 2015, a sand pump run on a wire line was used to remove loosened incrustation material. Approximately 14 feet of incrustation material was removed from the bottom of the well. The solid incrustation material was placed in an onsite poly 55-gallon drum and sampled for disposal purposes. Sample results indicated a detection of total petroleum hydrocarbons in the diesel range at 169 milligrams per kilograms (mg/kg) which is above the KAFB landfill limit of 100 mg/kg. The probable cause of the detection was determined to be FM32 dripper oil which fed the downhole pump and was floating on top of the groundwater inside the well.
- On November 13, 2015, a submersible pump was placed in the well and slightly less than two well casing volumes (approximately 5,000 gallons) was removed. The water was placed in an onsite storage tank prior to transportation and discharge to the BFF temporary treatment system.
- On November 20, 2015, an NMED-approved National Safety Foundation (NSF) flocculant certified for use in drinking water supply wells was used to ensure that solids settle out and turbidity is minimized prior to the post-rehabilitation video survey.
- On November 23, 2015, a downhole camera was used to provide a post-rehabilitation well video survey. DVDs of the video footage were provided to NMED. The video indicated that approximately half of the incrustation present before the rehabilitation had been removed and there was no visible damage to the casing. The brushing opened up some of the slots in the deeper part of the liner. The video shows a noticeable amount of floating particulate matter still in the water.
- On December 1 and 2, 2015, a V-Smart Injection Valve (downhole flow control valve) was installed in KAFB-7 with the top of the valve placed at approximately 560 feet.

References

Agarwal, R.G., 1980, A New Method to Account for Producing Time Effects When Drawdown Type Curves are Used to Analyze Pressure Buildup and Other Test Data. SPE Paper 9289 presented at the 55th SPE Annual Technical Conference and Exhibition, Dallas, Texas. September.

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Moench, A.F., 1997, Flow to a Well of Finite Diameter in a Homogeneous, Anisotropic Water-Table Aquifer. Water Resources Research, vol. 33, no. 6, pp. 1397 – 1407.

- U.S. Army Corps of Engineers (USACE), 2015a, Groundwater Disposition Letter Work Plan Addendum #1, Bulk Fuels Facility, Kirtland Air Force Base, New Mexico. Prepared by CB&I Federal Services, LLC for the USACE Omaha District under Contract No. W9128F-12-D-0003, Task Order 0025. October 30.
- U.S. Army Corps of Engineers (USACE), 2015b, Groundwater Disposition Letter Work Plan Addendum #2, Bulk Fuels Facility, Kirtland Air Force Base, New Mexico. Prepared by CB&I Federal Services, LLC for the USACE Omaha District under Contract No. W9128F-12-D-0003, Task Order 0025. November 9.

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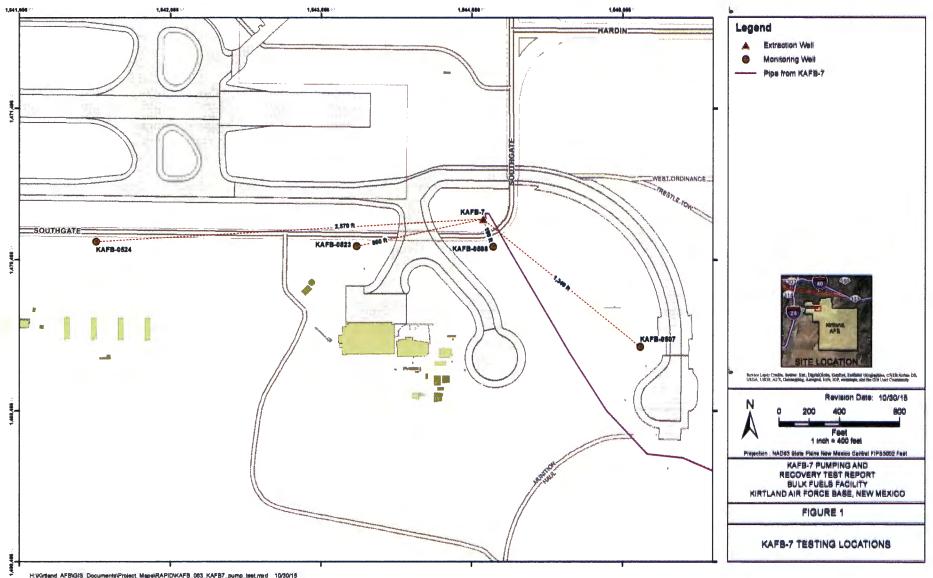
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FIGURES

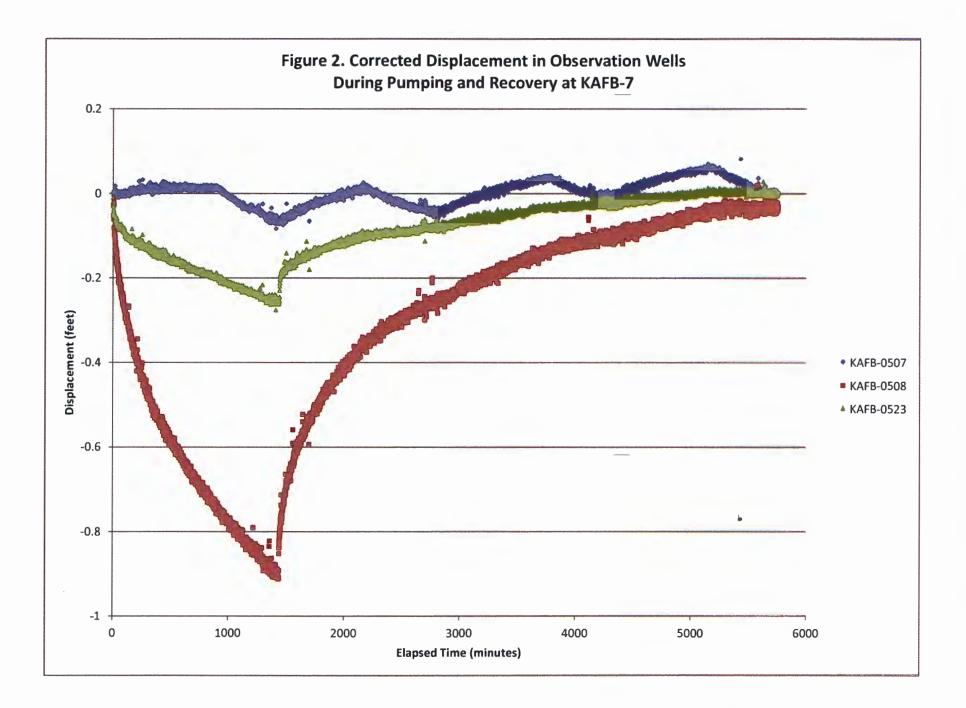
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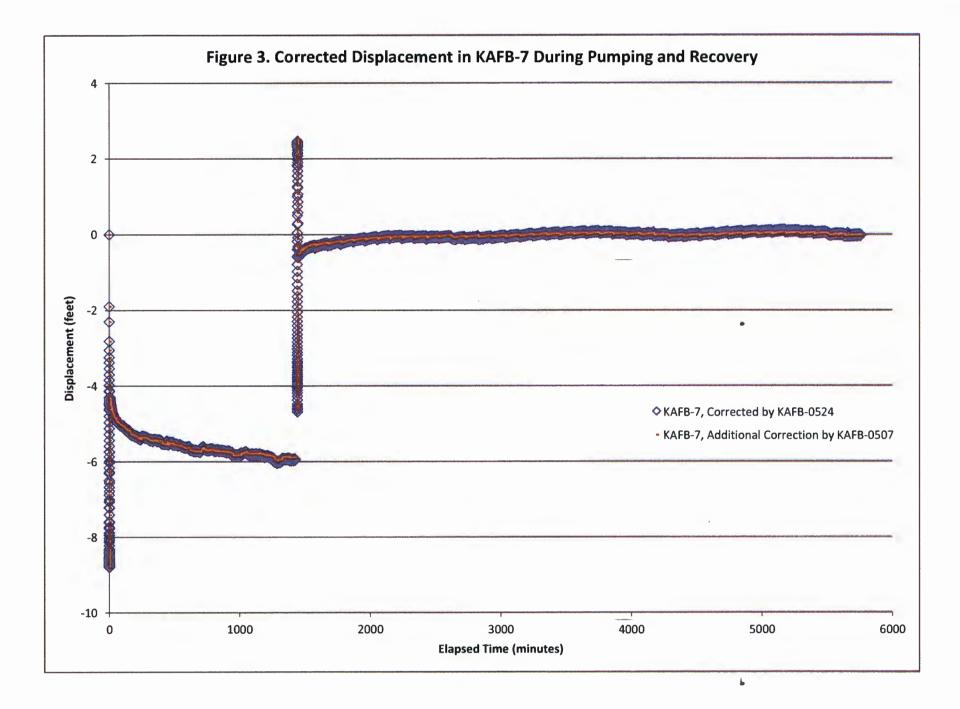
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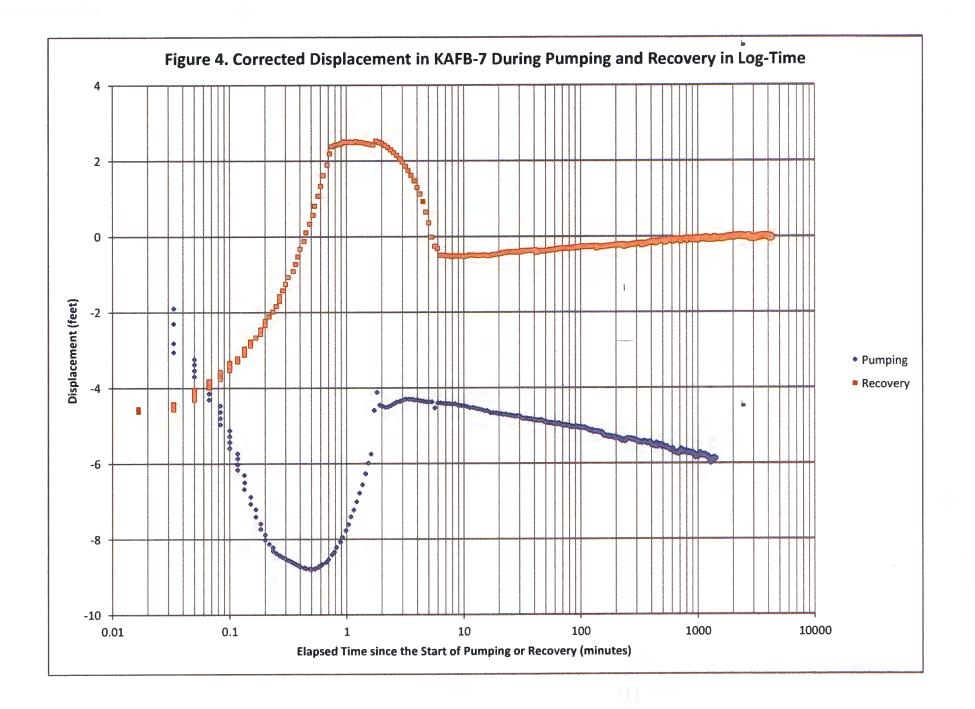


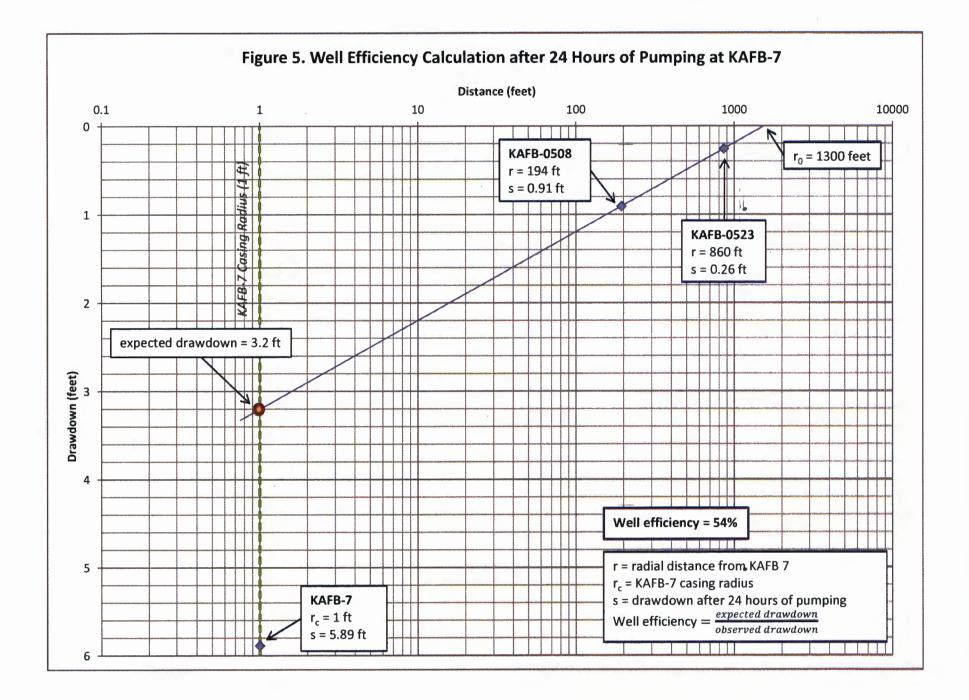
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TABLES

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Well ID	Screened Interval (feet bgs)	Depth to Groundwater (feet bgs)	Horizontal Distance From KAFB-7 (feet)	Observation Method ^a	Test Purpose	Transducer Log Setting True logarithmic with a maximum interval of 1 minute. Re-set at the start of recovery.		
KAFB-7		491	0	Pressure Transducer attached to Airline	Extraction Well			
KAFB-0507	482.3 to 507	491	1,340	Pressure Transducer	Observation Well	Linear, 1-minute intervals		
KAFB-0508	481 to 506	487	190	Pressure Transducer	Observation Well	Linear, 1-minute intervals		
KAFB-0523	600 to 625	482	860	Pressure Transducer	Observation Well	Linear, 1-minute intervals		
KAFB-0524	484 to 509	477	2,570	Pressure Transducer	Background Well	Linear, 1-minute intervals		

Table 1. KAFB-7 Pumping and Recovery Test Well Summary

^aIn-Situ Level TROLL^e 700 pressure transducers were used.

bgs - below ground surface

ID - identification

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	LOCATION CODE SAMPLE NO SAMPLE DATE SAMPLE PURPOSE				KAFB-7 RAPID-GW03 7-Oct-15 REG	
Chemical Class and Analytical Method ^a	Parameter	EPA MCLs ^b	NMED BG ^c	NMED GWPS ^d	Result	LOQ
Anions (mg/L)	BROMIDE				ND	0.2
Method SW9056A	CHLORIDE			250	10.3	0.
	NITRATE	10	4*	10	4.32	0.2
	NITRITE	1	4*		ND	0.2
	SULFATE			600	7-Oct-1 REG Result ND 10.3 4.32	2.
SM4500PE (mg/L)	O-PHOSPHATE (AS P)	1.5				0.0
Alkalinity (mg/L)	ALKALINITY, BICARBONATE				113	
Method SM2320B	ALKALINITY, CARBONATE				ATE 7-Oct-1 SE Result S0 Result S0 10.3 10 4.32 0 0.03 10 4.32 0 0.01 600 27.7 0 ND 600 27.7 0 ND 113 ND 0 113 0 ND 0 100 000 2255 000 80.7 100 ND 000 43.7 000 85 50 3.37 50 0.824 200	
	ALKALINITY, TOTAL	a that			113	
Alkalinity - Dissolved	ALKALINITY, BICARBONATE, LAB FILTERED				100	
(mg/L) Method SM2320B	ALKALINITY, CARBONATE, LAB FILTERED					
	ALKALINITY, TOTAL, LAB FILTERED	al la marte la			100	
TDS (mg/L) Method SM2540C	TOTAL DISSOLVED SOLIDS			1,000	225	2
Nitrogen (mg/L) Method EPA351.2	NITROGEN, KJELDAHL, TOTAL				ND	1.
DOC/TOC (mg/L) Method	DISSOLVED ORGANIC CARBON				ND	
SW9060A	TOTAL ORGANIC CARBON			la la constante de	RAPID-GW 7-Oci-13 REG Result ND 10.3 4.32 ND 27.7 ND 27.7 ND 113 ND 113 ND 113 ND 113 ND 113 ND 113 ND 100 0.30,37 3.37 5.710 2.28 ND ND 1.750 0.824 20,400 250 ND 3.03 3.6.4 1.4 ND	
Metals (µg/L) Method SW6010B	SILICON				14,000	4
Metals (µg/L)	ALUMINUM		_	5,000	80.7	5
Method SW6010C	ARSENIC	10		100	RAPID-G 7-Oct-1 Result ND 10.3 4.32 ND 27.7 ND 1103 4.32 ND 27.7 ND 1113 100 113 100 ND 1113 100 ND 114,000 80.7 ND 106 21.4 ND 36,600 2.357 ND 1,750 0.824 20,400 250 ND 3.03	2.
	BARIUM	2,000		1,000	106	1
	BORON		61	750	21.4	1
	CADMIUM	5		10		1.2
	CALCIUM				and the state in the second state of the secon	1,25
	CHROMIUM	100				2.
	COBALT					3.1
	COPPER	SAMPLE PURPOSE R EPA MCLs* NMED BG ° NMED GWPS d Result 10 4 * 10 4. 10 4 * 10 4. 10 4 * 10 4. 10 4 * 10 4. 10 4 * 10 4. 10 4 * 10 4. 10 4 * 10 4. 10 4 * 10 10 10 10.000 11 10. 10 10.000 14.0 10. 10 100 10. 10. 2.000 1,000 10. 10. 2.000 1,000 10. 10. 13.00 1,000 36.0 10. 13.00 1,000 36.0 10. 13.00 1,000 3. 5. 10.00 3. 3. 3. 20.0 20. 20. 20. <		2		
	IRON	_			and the second second second second second second	2
	LEAD	15	10	50	Constant of the second second second second	1.2
	MAGNESIUM	-		1.1.1		1,25
	MANGANESE					3.7
	MOLYBDENUM					
	NICKEL		ļ	200		2
	POTASSIUM	-			and a second second second second design and distances of the location.	1,25
	SELENIUM	50		50	and the second se	2
	SODIUM	-				1,25
	STRONTIUM					1
	THALLIUM	2				
	TITANIUM					0.1
	VANADIUM			10.000		3.1
	ZINC			10,000	30.4	-
Metals (µg/L) Method SW6020A	URANIUM	30		30	1.4	0.
Metals (µg/L) Method SW7470A	MERCURY	2		2	ND	0.
Metals (µg/L) Method SW6010B	SILICON, DISSOLVED				14,000	4

Table 2. Draft Analytical Sample Results

200	LOCATION CODE SAMPLE NO SAMPLE DATE SAMPLE PURPOSE					KAFB-7 RAPID-GW03 7-Oct-15 REG	
Chemical Class and Analytical Method ^a	Parameter	EPA MCLs*	NIMED BG [°]	NMED GWPS ^d	Result	LOQ	
Metals (µg/L)	ALUMINUM, DISSOLVED			5,000	75.7	5	
Method SW6010C	ARSENIC, DISSOLVED	10		100	0.961	2	
	BARIUM, DISSOLVED	2,000		1,000	112	1	
	BORON, DISSOLVED			750	RAPID-GI 7-Oct-1 REG Result 75.7 0.961	1	
	CADMIUM, DISSOLVED	5		ED NIMED GWPS ^d Result 5,000 75.1 100 0.96 1,000 112 750 22.2 10 NI 38,40 50 2.7 50 2.7 50 2.7 50 NI 1,000 2.1 1,000 NI 1,000 NI 2,100 NI 1,000 NI 1,000 NI 1,000 NI 2,100 NI 1,000 NI 2,000 NI 1,000 NI 2,000 NI 1,000 NI 2,000 NI 1,000 NI 2,000 NI 1,000 NI 2,000 NI	ND	1.2	
	CALCIUM, DISSOLVED				38,400	1,25	
	CHROMIUM, DISSOLVED	100		50	2.77	2.	
	COBALT, DISSOLVED			50	ND	3.1	
	COPPER, DISSOLVED	1,300		1,000	2.11	2	
	IRON, DISSOLVED			1,000	ND	2	
	LEAD, DISSOLVED	15	10	50	ND	1.2	
	MAGNESIUM, DISSOLVED				5,910	1,25	
	MANGANESE, DISSOLVED			200	0.988	3.7	
	MOLYBDENUM, DISSOLVED			1,000	ND		
	NICKEL, DISSOLVED			200	ND	2	
	POTASSIUM, DISSOLVED				1,810	1,25	
	SELENIUM, DISSOLVED	50		50	0.978	2	
	SODIUM, DISSOLVED		-		21,300	1,25	
	STRONTIUM, DISSOLVED				262	1.	
	THALLIUM, DISSOLVED	2				1	
	TITANIUM, DISSOLVED				Andhedister		
	VANADIUM, DISSOLVED					3.1	
	ZINC, DISSOLVED			10,000	7.6		
Metals (µg/L) Method SW6020A	URANIUM, DISSOLVED	30		30	1.3	0	
Metals (µg/L) Method SW7470A	MERCURY, DISSOLVED	2		2	ND	0	

Table 2. Draft Analytical Sample Results

* = The Value is the combination of Nitrate/Nitrite as Nitrogen

* = EPA analytical methods listed are for the most recent sampling event.

^b = EPA Maximum Contaminant Levels (MCLs) are from the EPA RSL Table, dated June 2015.

^e = New Mexico Environmental Department-HWB Approved Background Concentrations, SNL/Kirtland AFB, Chemical Constituents in Ground Water.

^d = New Mexico Environmental Department Ground Water Protection Standards (Sec. 20.6.2.3103)

EPA = Environmental Protection Agency

KAFB = Kirtland Air Force Base

LOQ = Limit of Quantitation

µg/L = microgram per liter

mg/L = milligram per liter

ND = Not detected.

RSL = Regional Screening Level.

Shading indicates the analyte was detected.

Table 3. Aquifer Properties Analysis Results

Well ID	Pumping or Recovery	Transmissivity (feet ² /day)	Hydraulic Conductivity (feet/day)	Hydraulic Conductivity (gpd/foot ²)	Specific Yield (dimensionless)	Specific Storage (per foot)	Storativity (dimensionless)
KAFB-7	Pumping	35,000	100	750	0.001	3.84E-10	1.40E-07
NAFD-7	Recovery	38,000	100	750	0.0026	1.40E-08	5.00E-06
	Pumping	54,000	150	1,100	0.0079	2.49E-05	1.70E-02
KAFB-0508	Recovery	28,000	80	600	0.038	2.11E-05	7.70E-03
KAFB-0523	Pumping ^a	110,000	300	2,200	0.033	2.74E-06	1.00E-03
NAP 0-0523	Recovery	21,000	60	450	0.066	8.30E-07	3.00E-04
Geometric Mean of Results ^b	Pumping and Recovery	34,000	90	670	0.027	7.6E-06	3.4E-03

^aThe pumping results for KAFB-0523 were not used to calculate the geometric mean of results. During the recovery period, a separate analysis of the first 24 hours of recovery in KAFB-0523 yielded results consistent with the pumping period. However, the shape of the recovery curve continued to change after that point, and the analysis of the entire recovery curve yielded results more consistent with those determined in KAFB-0508 during pumping and recovery.

^bSpecific yield, specific storage, and storativity calculated using KAFB-7 data were not used to calculate the geometric mean of results, as storage parameters are more accurate when calculated using both pumping and observation wells.

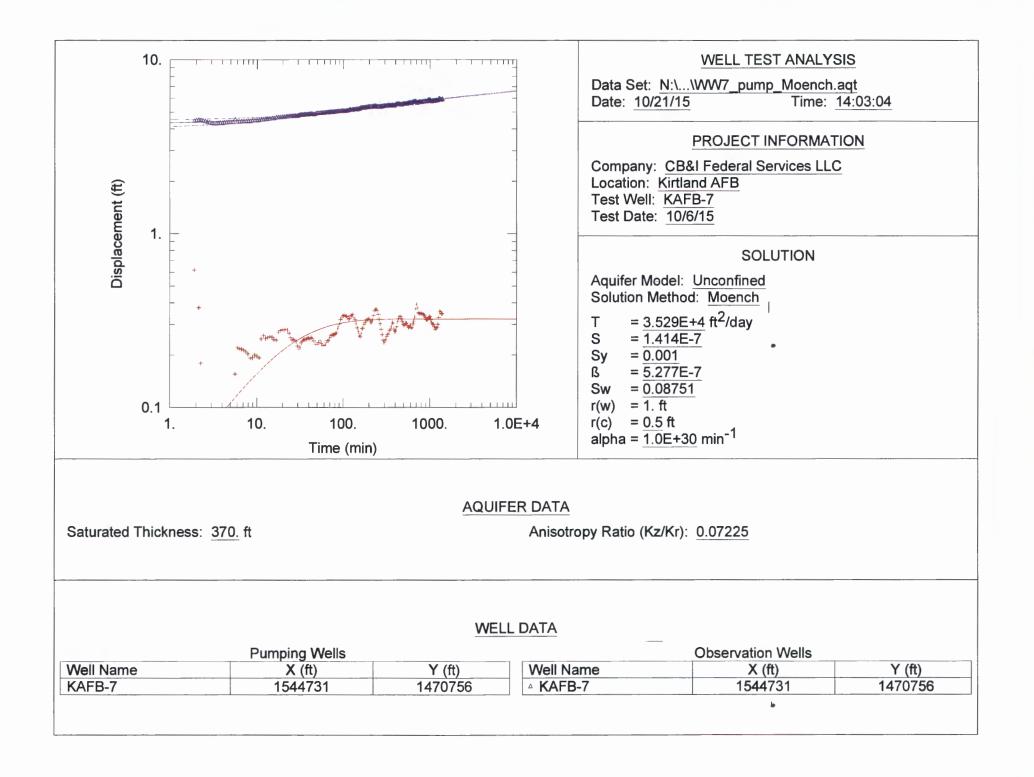
gpd - gallons per day

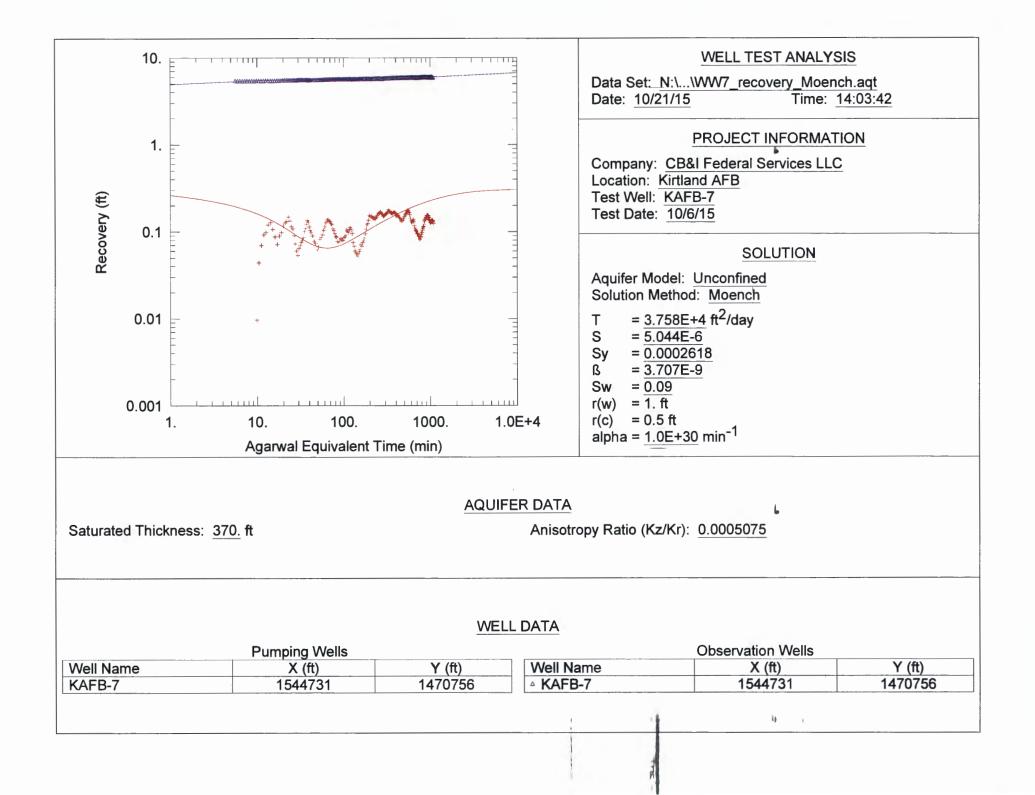
ID - identification

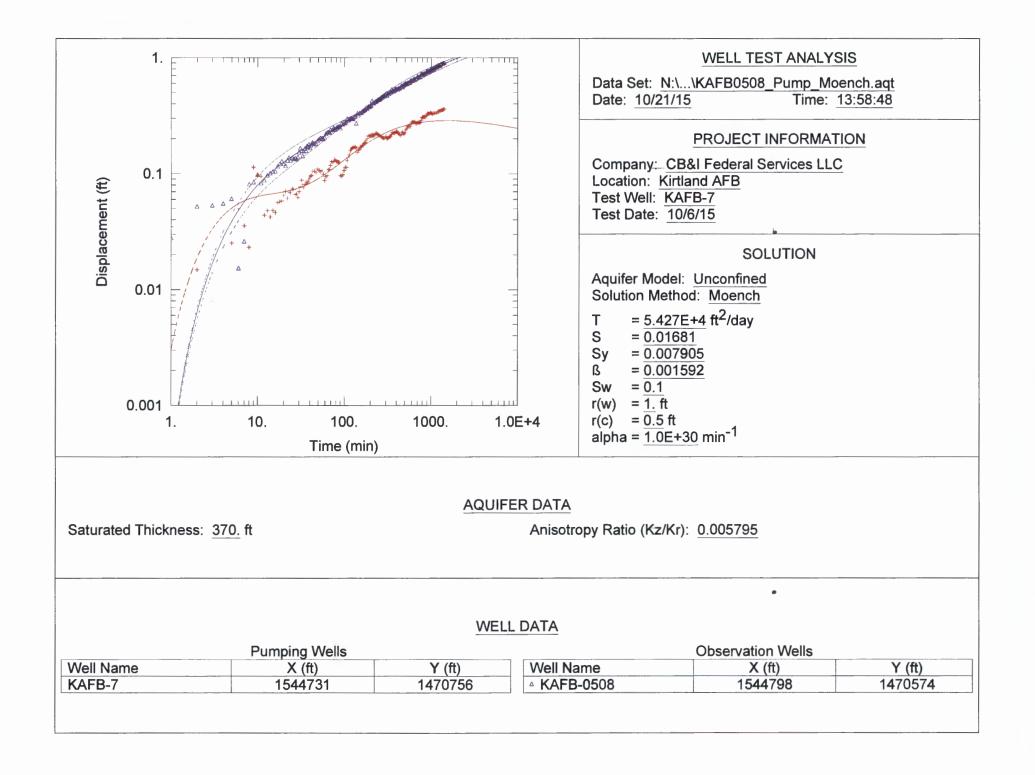
ATTACHMENT 1

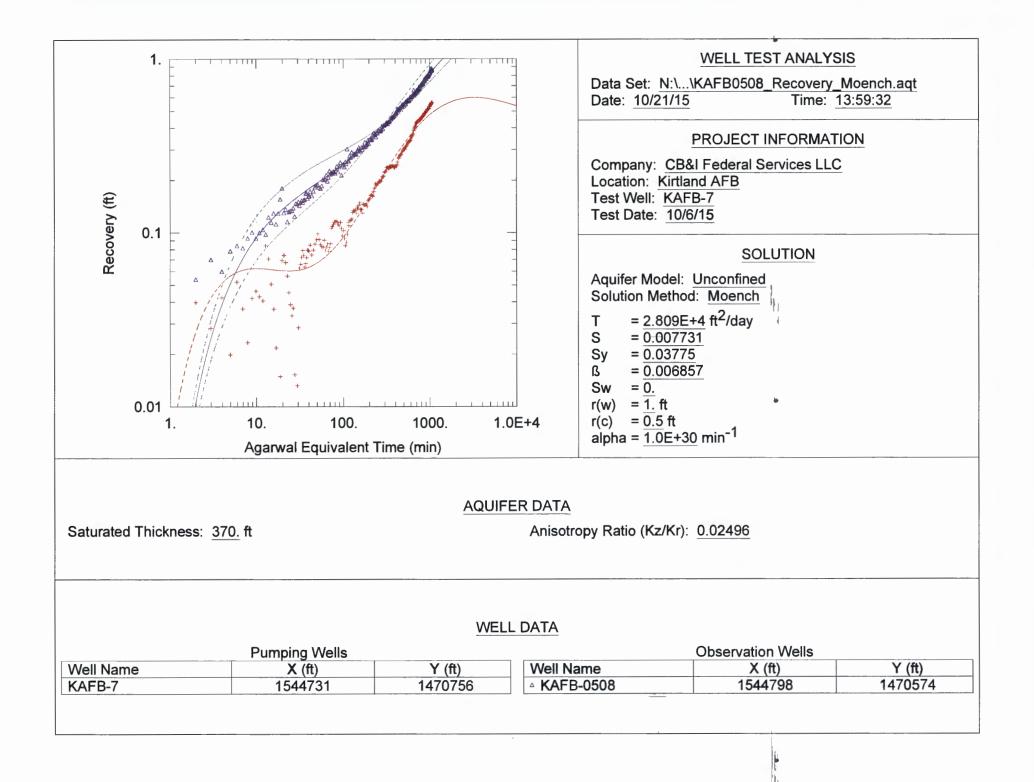
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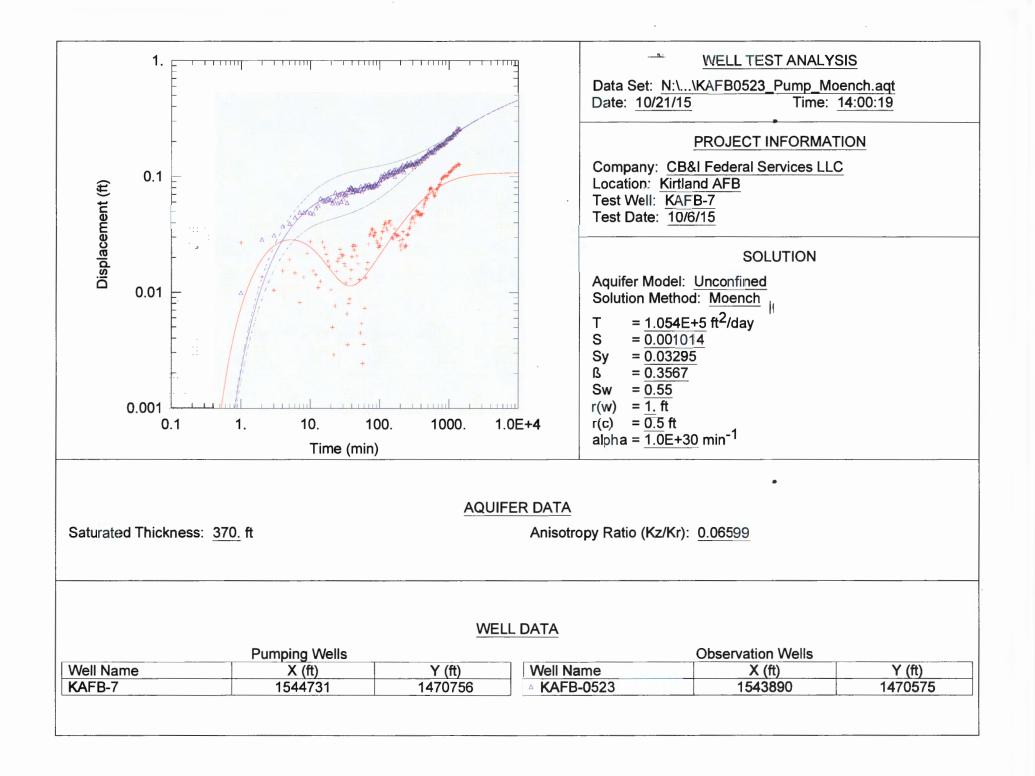
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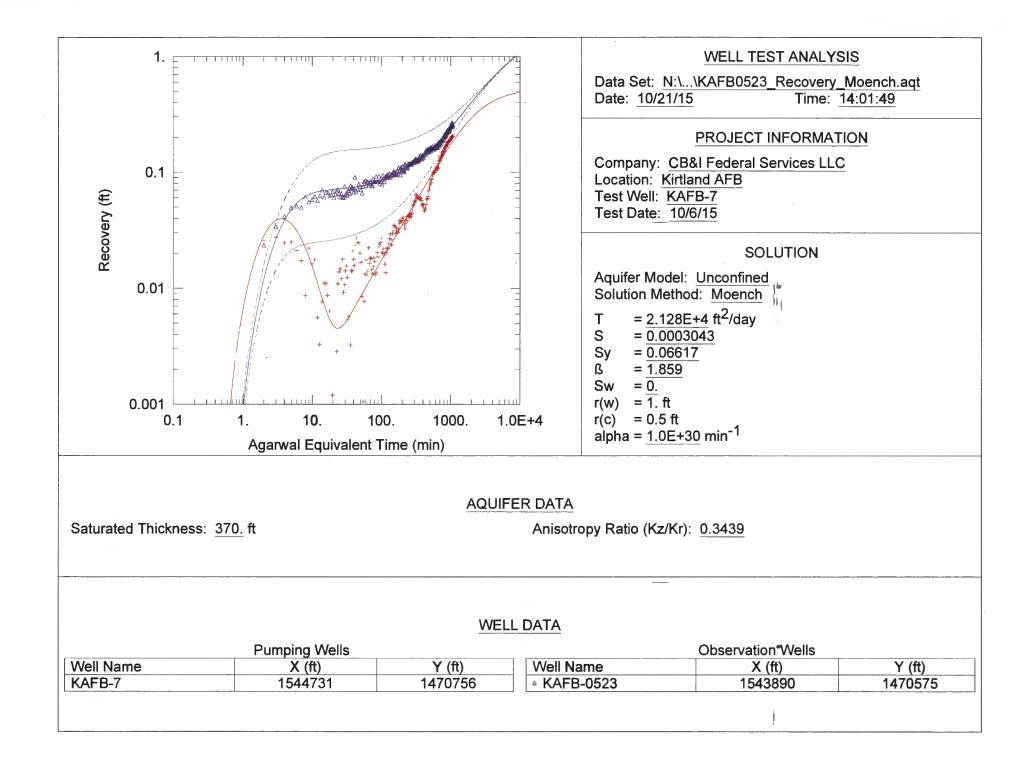


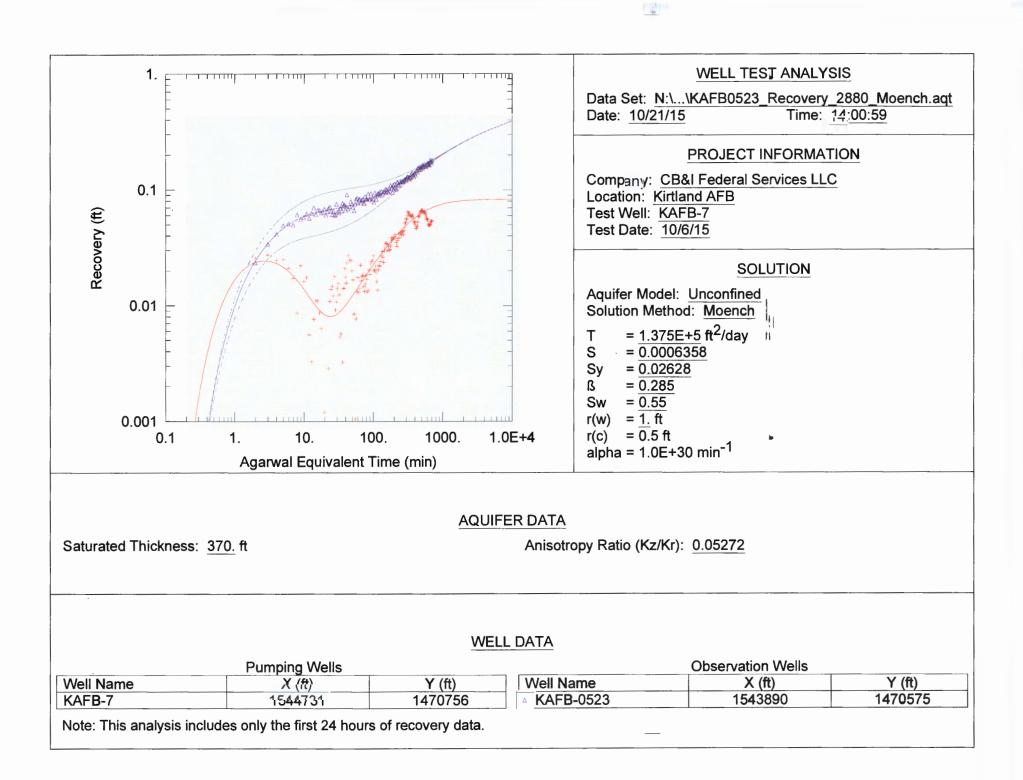












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