# IN THE MATTER OF SPARTON TECHNOLOGY, INC. U.S. EPA DOCKET NO. RCRA-VI-001 (H)-96-H

## REPORT OF PIERCE L. CHANDLER, JR., ON GEOLOGY/HYDROGEOLOGY CHARACTERIZATION, CONTAMINANT PLUME CHARACTERIZATION, RISK ASSESSMENT, AND AQUIFER RESTORATION SPARTON TECHNOLOGY COORS ROAD FACILITY ALBUQUERQUE, NEW MEXICO

#### February 4, 1997

The following report is my analysis and conclusions on the characterization of subsurface conditions and a "contaminant plume" and the resulting assessment of risk/threat posed to human health. The potential for aquifer restoration is also evaluated with respect to site-specific conditions, risk/threat, and technical practicability.

My report is based on my training, education, and experience as a professional engineer and hydrogeologist with particular emphasis on water resource and solid/ hazardous waste projects. A copy of my curriculum vitae is attached.

A significant portion of my previous work has been on sites regulated under the Resource Conservation and Recovery Act (RCRA) of 1976 and subsequent amendments. With respect to the Sparton site, I was the principal investigator and author of the RCRA Facility Investigation (RFI) Report (Sparton, 1992), the Corrective Measures Study (CMS) Report (Sparton, 1996), and the Effectiveness of the Groundwater Recovery Well System in the Upper Flow Zone (Effectiveness) Report (Sparton, 1995).

On the basis of education, training, general experience, and specific experience at the Sparton Coors Road Facility, I am qualified to make the conclusions and statements expressed in the following report.

### GEOLOGY/HYDROGEOLOGY CHARACTERIZATION

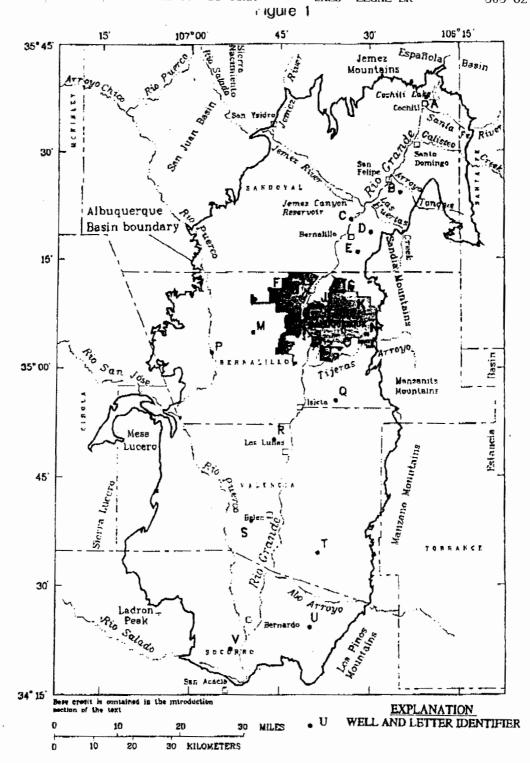
The geology/hydrogeology of the Albuquerque area is well understood and well documented. The Sparton facility is located within the most extensively studied and modelled part of the Albuquerque area. Figure 1 is a map of the Albuquerque Basin and its relative location with respect to the City.

A detailed discussion of geologic/hydrogeologic characterization with supporting maps and references can be found in the 1992 RCRA Facility investigation (RFI) Report submitted by Sparton. The RFI information was updated in Sparton's 1996 Corrective Measures Study (CMS) Report to include the most recent information developed by USGS, USBR, New Mexico Water Resources Research Institute (NMWRRI) and others. The 1996 CMS Report also contains an extensive bibliography arranged by subject.

Regional. The geology and hydrogeology of the Albuquerque Basin in central New Mexico has been extensively studied, modelled, and documented since at least 1930. This wealth of information has been used to assemble both a conceptual model (USGS, 1993 and USBR, 1996) and a three-dimensional finite-difference groundwater flow model of the Albuquerque Basin (USGS, 1995). These models are the essential tools used in all water resource planning and management in the Albuquerque Basin. However, as Peter Balleau (NMWRRI, 1995) points out, the current understanding of the Basin is remarkably consistent with the historic understanding of the Basin.

The aquifer consists of complex, layered, and interbedded sedimentary basin and valley filling of five deep structural depressions in the Rio Grande Rift. The resulting geology is characterized by heterogeneous and anisotropic conditions throughout the aguifer and includes gravels, sands, silts, and clays.

With respect to hydrogeology, the main source of groundwater (recharge) is from the Rio Grande and adjacent irrigated agriculture. Horizontal hydraulic



--Location of selected wells in the Albuquerque Basin, Central New Mexico.

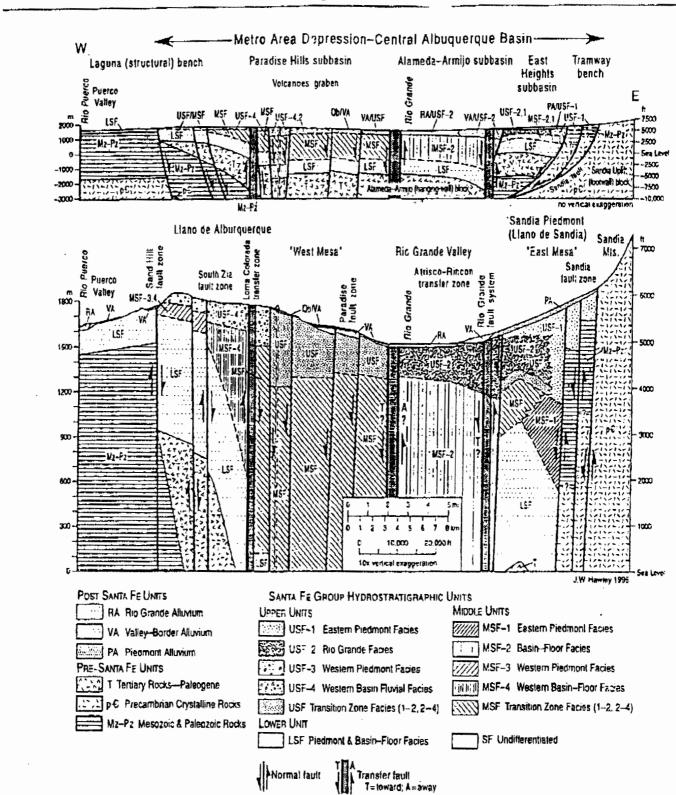
conductivity ranges from 0.15 feet/day to 70 feet/day with the higher hydraulic conductivities on the east side of the river. Due to the substantial anisotropy, vertical hydraulic conductivities are 1/200 to 1/1000 of horizontal values. Hydraulic gradients range from approximately 0,001 to 0,007 with the higher gradients along the mountain front east of the river and/or associated with heavily pumped well fields. However, the great variation in hydraulic conductivity is the most significant influence on the direction and rate of groundwater movement.

Regional conditions have been determined through the large number of groundwater investigations (and wells) that have been conducted throughout the basin. There are also numerous exposures created by both erosional forces and by man-made construction. In addition, the flow model has been sufficiently calibrated to serve as a predictive tool.

Local Conditions. West of the river, sediments are generally finer, hydraulic conductivities are lower, and hydraulic gradients are flatter (USGS, 1995). An excellent depiction of local conditions is shown in the west-east cross-section along Paseo de Norte Boulevard (USBR, 1996) included as Figure 2.

Local conditions west of the river and to the north of Paseo de Norte have been documented by: municipal production well records; private well installations; pump testing (Intel Shomaker & Assoc., 1995, 1996); exposures along the Calabacillas Arroyo; and the numerous monitoring wells installed by Sparton. Dr. John Hawley, of the Middle Rio Grande Water Assessment Team, believes that the Sparton plume characterization is the best groundwater tracer test conducted in the Albuquerque area and defines the local groundwater flow rate and direction.

Site-Specific. Site geologic/hydrogeologic conditions are remarkably similar to regional and local characterization. Subsurface conditions are extremely heterogeneous and anisotropic as clearly shown by comparison of boring logs for wells completed at different locations and particularly by comparison of boring logs at cluster well locations where several wells are installed in very close proximity. An excellent example is well cluster 9. Using boring logs for



—A cross section of the Metro Area Depression in the central Albuquerque Basin showing relative thickness and discontinuity of the Upper, Middle, and Lower Santa Fe Group and valley fill aquifer systems. groundwater monitoring wells MW-48, MW-55, and MW-56 (RFI Report, 1992) it is obvious that subsurface conditions vary significantly over short horizontal and vertical distances. Other logs and/or clusters show similar variation.

Hydraulic conductivity has been defined by multiple-well pump testing and the resulting range of 21 to 32 feet/day matches regional values. Documentation and detailed analyses of the pump testing are given in Attachment 10 of the 1992 RFI Report. Hydraulic gradients (and the impact of season, precipitation and irrigation of adjacent fields) have been determined from an extensive, long-term data base of water level readings from numerous groundwater monitoring wells. Water level data through June 1991 is summarized in the RFI Report. Post-RFI water level data and summarizing information is contained in the 1996 CMS Report. Current water level contours are shown on Figure 3. Average gradient is approximately 0.002 which matches well with regional characterization.

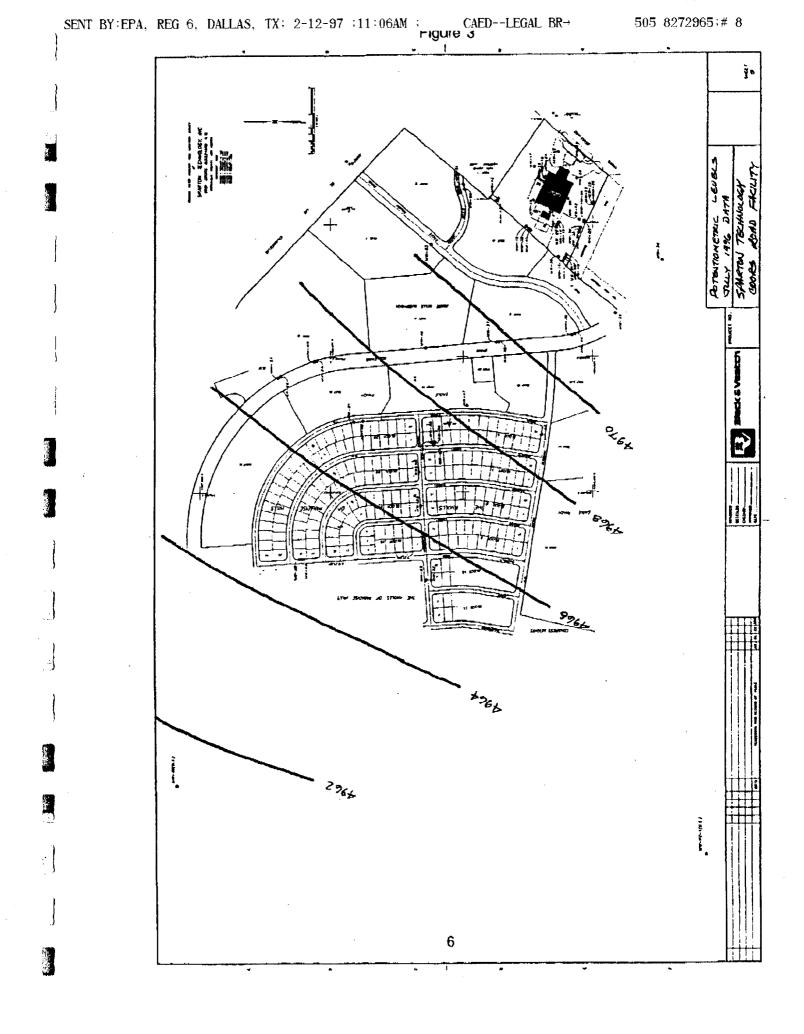
Flow direction has been determined to be to the west-northwest at a rate of less than 100 feet per year based on the hydraulic parameters. The plume "tracer" confirms this assessment. Regionally, flow was predicted to be more westerly to southwesterly in the area. This difference is the result of much higher density well spacing on the Sparton site (hundreds of feet) as compared to the regional well spacing (miles).

Irrigation of the adjacent farmland to the east of the site has a seasonal 2- to 3-foot impact on groundwater levels in wells close to the fields. However, to the west of the Sparton property, water levels are unaffected. Over the last five or six years, overall water levels have dropped one to two feet; however, gradients and direction are relatively unchanged.

Site conditions have been verified by extensive site investigations conducted since 1983. These investigations include:

- 1. Seventy-two groundwater monitoring well installations;
- Eleven soil boring installations;
- Multiple pumping tests (multi-well and single well);
- 4. Geophysical logging:

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- 5. Geotechnical classification;
- Extended monitoring of water levels and contaminant concentrations;
- 7. Extensive research of published literature and anecdotal information; and
- 8. Observation of geologic exposures in immediate area.

### Need For Additional Site-Specific Study

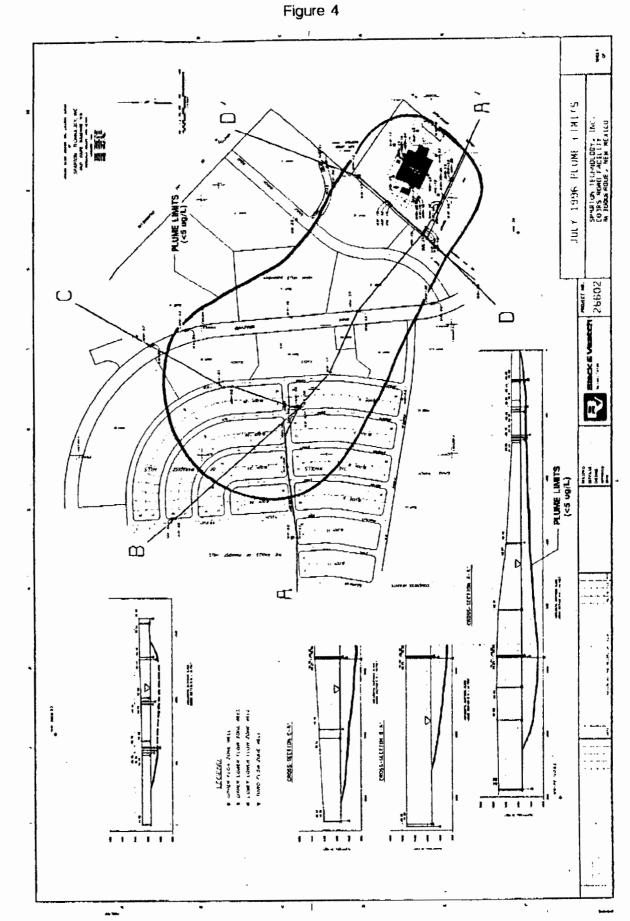
The Albuquerque Basin has been extensively studied and characterization has been developed to the point that long-range projections and modifying impacts can be modelled with confidence. Characterization of the Sparton site is even more detailed and serves as a microscopic view of the upper part of the Basin.

Additional investigation is not needed to fill information/data gaps. The existing characterization is more than sufficient to define, with reasonable certainty, geologic and hydrogeologic conditions at the site. The existing information is also more than adequate for design purposes. Additional investigation would only generate more confirming data at a cost premium.

### **CONTAMINANT PLUME CHARACTERIZATION**

The chlorinated solvent plume at the Sparton facility is well-characterized and understood. Plume constituents are primarily Trichlorethylene (TCE) with lesser concentrations of 1,1,1 - Trichloroethane (TCA), 1,1 - Dichloroethylene (DCE), and Dichloromethane (DMA). Concentration and/or presence of TCE is most appropriate for describing the plume. TCE is the most consistently and commonly detected constituent and also is found at the highest concentration. During preparation of the RFI Report; TCE also had the lowest drinking water MCL of 0.005 mg/l.

The current extent of the plume (July 1996 sampling and analysis) is clearly shown on Figure 4. As discussed in subsequent paragraphs of this section, plume mechanics have been confirmed by extensive investigation and comparison to detailed hydrogeologic characterization for the area. The plume definition is more than adequate to assess potential risk/threat and for any needed remedial design purposes.



A detailed discussion of the plume characterization is contained in the 1992 RFI Report. Updated plume information covering the period from June 1991 through early 1996 is detailed in the 1996 CMS Report.

In subsequent investigation in summer of 1996, the CMS report conclusions on plume extent and rate of migration were confirmed by installing five groundwater monitoring wells (MW-65, MW-66, MW-67, MW-68, and MW-69). Well locations were chosen to show that the plume limits presented in the CMS Report were realistic and that direction and rate of migration conclusions were valid. The five wells were installed outside and/or below the leading edge of the plume defined in the CMS Report. Not surprisingly, all five wells were non-detect.

The ability to predict results in advance of installation demonstrates the comprehensive understanding of the plume. Further, as discussed in subsequent sections, the five new wells, together with the updated data base, effectively address and answer EPA's concerns on plume characterization numbered 3, 5, 7, and 9 in their June 20, 1996, Technical Review of the CMS Report.

Extent. Consistent with the documented vertical anisotropy and dominance of horizontal groundwater flow, the plume horizontal extent (approximately 2,600 feet downgradient and 3300 feet overall) is much greater than plume depth (nominally 50 to 125 feet). Plume width is significant (approximately 1,650 feet) due to the low groundwater flow rates and to the heterogeneous subsurface conditions. Plume currently covers about 90 acres.

A total of 72 groundwater monitoring wells have been installed at the site since 1983. There are currently 57 active wells including 8 on-site wells converted to recovery well operation. The 49 monitoring wells have been installed at horizontal locations as shown on Figure 4. Wells have also been installed at various penetration depths into the aquifer. Well depth is shown by legend symbol on the Figure. The nomenclature is as follows:

1. Upper flow zone (UFZ) indicates well is screened across the top of the aquifer.

- 2. Upper lower flow zone (ULFZ) indicates well is approximately 30 feet below the top of the aquifer.
- 3. Lower lower flow zone (LLFZ) indicates well is approximately 60 feet below the top of the aquifer.
- 4. Third flow zone (TFZ) indicates well is 75 to 175 feet into the aquifer.

A summary of all wells including flow zone identification and completion intervals is included as Table 1.

The use of flow zones is for vertical location purposes only. At 13 locations, wells completed in different flow zones have been clustered together to provide vertical definition.

The extent of the plume is defined by detection wells (TCE concentration greater than 5  $\mu$ g/l) inside the plume and by non-detection wells outside and/or below the plume. TCE concentration histories for each of the monitoring wells are given in Table 2. In 1996, 23 of the 49 wells were below 5  $\mu$ g/l. These non-detect wells have been circled on Figure 5 to show their relationship to the defined plume limits.

The detect vs non-detect delineation of the plume is further confirmed by the approximately normal or Gaussian distribution of TCE concentration across any given cross-section of the plume. For example:

- Transverse UFZ section across the leading edge of the plume (wells MW-62, MW-48, MW-61 and MW-57) shows range from non-detect to 1900 µg/l and back to non-detect.
- Transverse UFZ section at mid-plume (wells MW-62, MW-37, MW-63) shows range from non-detect to 720 µg/l to non-detect.

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# Table 1

# WELL SUMMARY

FN-1     OTZ     5044.54     60.0     70.0     4984.54     4974.54     10.0       7     OTZ     5044.11     62.5     68.5     4981.61     4976.51     5.0       12     OTZ     5042.58     64.0     74.0     4976.58     4976.51     5.0       13     OTZ     5041.25     60.0     70.0     4981.25     4971.25     10.0       14     OTZ     5047.64     60.0     70.0     4981.25     4971.25     10.0       15     OTZ     5047.64     60.0     70.0     4981.25     4971.25     10.0       16     OTZ     5047.64     64.0     71.0     4971.58     4971.35     10.0       17     OTZ     5045.58     67.0     72.0     4982.79     4971.78     10.0       20     CLTZ     5048.56     64.5     69.5     4981.66     4978.86     5.0       21     OTZZ     5048.70     67.7     72.7     4980.30     4971.31     5.0       22	WELL NUMBE		ONE .	NEASUR 18G POINT ELEVATION	DEPTE TO TOP OF SCREEN (FT.)	DEFTE TO BOTTOM OF SCREEN (FT.)	ELEVATION AT TOP OF SCREEN (FT., NSL)	ELEVATION A BOTTON OF SCREEN (FT., MSL)	T LENGTH OF SCREEN (FT.)
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9     0TZ     5043.53     64.0     74.0     4981.61     4976.51     5.0       12     0TZ     5043.25     60.0     70.0     4983.25     4973.25     10.0       14     0TZ     5043.25     60.0     70.0     4983.25     4973.25     10.0       15     0TZ     5047.45     60.0     70.0     4987.45     4977.45     10.0       16     0TZ     5047.45     60.0     71.0     4987.45     50.0     50.0       17     0TZ     5045.58     68.0     78.0     4977.58     4977.58     10.0       19     0TZ     5046.55     97.0     107.0     4982.25     4933.25     10.0       10     0TZ     5046.36     64.5     69.5     4931.64     4970.75     10.0       10     0TZ     5048.36     67.7     77.0     4976.51     4971.51     5.0       20     0TZ     5048.50     67.0     72.7     4981.30     4975.30     5.0       21 <td< td=""><td>• •</td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>	• •	-							
12     UTZ     5043.25     64.0     74.0     4978.38     4968.38     10.0       13     UTZ     5043.25     60.0     70.0     4981.25     4973.25     10.0       14     UTZ     5041.51     61.5     71.5     4980.25     4973.25     10.0       15     UTZ     5047.36     68.0     73.0     4977.49     4977.43     10.0       16     UTZ     5045.58     68.0     73.0     4977.38     4977.38     10.0       19     ULTZ     5045.58     68.0     78.0     4977.38     4977.38     10.0       20     LLTZ     5046.77     125.0     138.0     4970.73     4977.51     5.0       21     UTZ     5048.06     72.0     77.0     4974.06     4971.05     5.0       22     UTZ     5048.06     67.0     72.7     4980.30     4973.30     5.0       23     UTZ     5045.71     73.0     78.0     4977.1     5.0     5.0       24 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>									
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24     UTZ     5048.70     68.4     73.4     4980.30     4975.30     5.0       25     UTZ     5049.00     67.7     72.7     4981.30     4976.10     5.0       26     UTZ     5045.50     67.0     72.0     4972.71     4967.71     4567.71     5.0       27     UTZ     5044.550     67.0     72.0     4978.50     4973.50     5.0       28     UTZ     5044.51     103.0     113.0     4971.69     4972.69     5.0       29     ULFZ     5044.70     97.0     107.0     4947.70     4937.70     10.0       30     ULFZ     5044.70     97.0     107.0     4941.05     4930.50     10.0       31     ULFZ     5044.23     63.0     73.0     4981.29     4971.29     10.0       33     GTZ     5044.23     63.2     73.2     4979.30     10.0       34     OTZ     5044.23     63.2     73.2     4979.30     10.0       34     DTZ									
25     0P2     5049.00     67.7     72.7     4981.30     4976.30     5.0       26     0P2     5045.71     73.0     74.0     4972.71     4967.71     5.0       27     UPZ     5043.50     67.0     72.0     4978.50     4973.50     5.0       28     UPZ     5044.65     65.0     70.0     4976.50     4972.69     5.0       29     ULPZ     5044.51     103.0     113.0     4941.51     4931.51     10.0       30     ULPZ     5044.70     97.0     107.0     4947.53     4937.70     10.0       31     ULPZ     5044.73     97.0     106.0     4940.05     4930.05     10.0       33     GPZ     5044.29     63.0     73.0     4971.29     10.0       34     OPZ     5043.49     65.5     66.5     977.99     4967.95     10.0       35     OPZ     5043.53     92.3     92.3     4971.29     10.0     0       36     OPZ     5	-								
26   UFZ   5045.71   73.0   78.0   4972.71   4967.71   5.0     27   UFZ   5042.69   65.0   70.0   4978.50   4973.50   5.0     28   UFZ   5044.51   103.0   113.0   4941.51   4931.51   10.0     30   ULFZ   5044.51   103.0   113.0   4941.51   4937.70   10.0     31   ULFZ   5044.53   96.0   106.0   4947.73   4937.53   10.0     32   LLFZ   5048.05   108.0   118.0   4941.51   4937.53   10.0     33   0FZ   5042.50   63.0   73.0   4981.29   4971.27   10.0     34   0FZ   5042.50   63.2   73.2   4979.10   4967.99   10.0     35   0FZ   5042.50   63.2   73.2   4977.99   4967.05   10.0     36   0FZ   5039.35   82.3   92.3   4977.05   4967.05   10.0     37   0FZ   5044.05   123.0   133.0   4921.06   40.0   0.0									
27     UFZ     5045.50     67.0     72.0     4978.50     4973.50     5.0       28     UFZ     5042.69     65.0     70.0     4977.69     4972.69     5.0       29     ULFZ     5044.51     103.0     113.0     4941.51     4931.51     10.0       30     ULFZ     5044.70     97.0     107.0     4947.76     4937.70     10.0       31     ULFZ     5048.05     108.0     118.0     4947.53     4937.53     10.0       32     LLFZ     5044.29     63.0     73.0     4981.29     4971.29     10.0       33     OFZ     5034.49     56.5     66.5     4977.99     4967.99     10.0       35     OFZ     5035.35     52.3     92.3     4977.05     4967.05     10.0       36     UFZ     5044.29     63.12     73.2     4979.30     4969.30     10.0       35     OFZ     5035.35     125.0     1976.66     4946.64     10.0       36     LLFZ </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>									
28     UTZ     5042.69     65.0     70.0     4977.69     4972.69     5.0       29     ULFZ     5044.51     103.0     113.0     4941.51     4931.51     10.0       30     ULFZ     5044.70     97.0     107.0     4947.70     4937.70     10.0       31     ULFZ     5043.53     96.0     106.0     4947.73     4937.53     10.0       32     LLFZ     5048.05     108.0     118.0     4940.05     4937.99     10.0       33     OFZ     5042.50     63.2     73.2     4971.29     10.0       34     OFZ     5039.35     82.3     92.3     4977.05     4969.30     10.0       35     OFZ     5059.35     82.3     92.3     4977.82     4967.05     10.0       36     OFZ     5039.35     82.3     92.3     4976.66     4966.66     10.0       35     UFZ     5044.32     126.5     136.5     4917.82     4907.82     10.0       36     UFZ <td>-</td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	-	-							
29     ULFZ     5044.51     103.0     113.0     4941.51     4931.51     10.0       30     ULFZ     5044.70     97.0     107.0     4947.70     4937.70     10.0       31     ULFZ     5043.53     96.0     106.0     4947.70     4937.53     10.0       31     ULFZ     5048.05     106.0     118.0     4940.05     4930.05     10.0       33     GPZ     5044.29     63.0     73.0     4981.29     4971.79     10.0       34     GPZ     5034.49     56.5     66.5     4977.99     4967.99     10.0       35     GPZ     5034.32     63.2     73.2     4979.30     4967.95     10.0       36     GPZ     5039.35     82.3     927.05     4967.05     10.0       37     UPZ     5091.66     115.0     125.0     4976.66     4966.66     10.0       38     LLFZ     5044.05     123.0     133.0     4921.06     4911.06     10.0       40     t									
30     TLF2     5044.70     97.0     107.0     4947.70     4937.70     10.0       31     TLF2     5043.53     96.0     106.0     4947.53     4937.70     10.0       32     LLFZ     5048.05     108.0     118.0     4940.05     4930.05     10.0       33     GFZ     5044.29     63.0     73.0     4981.29     4971.79     10.0       34     GFZ     5044.39     56.5     66.5     4977.99     4967.99     10.0       35     GFZ     5042.50     63.2     73.2     4979.30     4969.30     10.0       36     GFZ     5039.35     82.3     92.3     4977.65     4967.65     10.0       37     GFZ     5044.32     126.5     136.5     4917.82     4907.82     10.0       38     LLFZ     5044.05     123.0     137.0     4926.35     491.06     10.0       41     ULFZ     5046.77     92.0     97.0     4954.77     4945.77     5.0       42									
31     ULFZ     5043.53     96.0     106.0     4947.53     4937.53     10.0       32     LLFZ     5048.05     100.0     118.0     4940.05     4930.05     10.0       33     GFZ     5044.29     63.0     73.0     4981.29     4971.29     10.0       34     GFZ     5042.50     63.2     73.2     4979.30     4967.95     10.0       35     GFZ     5042.50     63.2     73.2     4979.30     4967.05     10.0       36     GFZ     5039.35     82.3     92.3     4977.05     4967.05     10.0       37     OFZ     5091.66     115.0     125.0     4976.86     4961.06     10.0       38     LLFZ     5044.06     123.0     133.0     4921.06     4921.06     10.0       40     .LFZ     5044.07     92.0     97.0     4926.35     4915.15     10.0       41     ULFZ     5046.77     92.0     97.0     4930.74     4920.74     10.0       4									
32     LLPZ     5048.05     108.0     118.0     4940.05     4930.05     10.0       33     GFZ     5044.29     63.0     73.0     4981.29     4971.29     10.0       34     GFZ     5034.49     56.5     66.5     4977.99     4967.99     10.0       35     GFZ     5042.50     63.2     73.2     4979.30     4969.30     10.0       36     GFZ     5039.35     82.3     92.3     4977.05     4969.30     10.0       37     GFZ     5091.66     115.0     125.0     4976.66     4966.64     10.0       38     LLFZ     5044.32     126.5     136.5     4917.82     4907.82     10.0       41     GLFZ     5044.06     123.0     133.0     4921.06     4910.0     10.0       42     GLFZ     5044.77     92.0     97.6     4954.33     4942.33     10.0       41     GLFZ     5045.71     127.0     137.0     4952.71     4949.77     5.0									
33     GPZ     5044.29     63.0     73.0     4981.29     4971.29     10.0       34     GPZ     5034.49     56.5     66.5     4977.99     4967.99     10.0       35     GPZ     5042.50     63.2     73.2     4979.30     4967.99     10.0       36     GPZ     5039.35     82.3     92.3     4977.05     4967.05     10.0       37     GPZ     5039.35     82.3     92.3     4977.05     4967.05     10.0       38     LLPZ     5044.32     126.5     136.5     4917.82     4907.82     10.0       39     LLPZ     5044.05     123.0     133.0     4921.06     491.06     10.0       40     .LLPZ     5045.77     92.0     97.0     4954.33     4942.33     10.0       41     ULPZ     5057.33     105.0     115.0     4952.71     4949.77     5.0       42     ULPZ     5057.74     127.0     137.0     4930.74     4920.74     10.0       4									
34     0FZ     5034.49     56.5     66.5     4977.99     4967.99     10.0       35     0FZ     5042.50     63.2     73.2     4979.30     4969.30     10.0       36     0FZ     5059.35     82.3     92.3     4977.05     4967.05     10.0       37     0FZ     5091.66     115.0     125.0     4976.66     4966.66     10.0       38     LLFZ     5044.32     126.5     136.5     4917.82     4907.82     10.0       39     LLFZ     5044.06     123.0     133.0     4926.35     4916.35     10.0       40     .LFZ     5044.05     123.0     137.0     4926.35     4916.35     10.0       41     ULFZ     5045.71     127.0     137.0     4926.35     4916.35     10.0       42     ULFZ     5057.74     127.0     137.0     4930.74     4920.74     10.0       43     LLFZ     5058.71     106.0     116.0     4952.71     4942.71     10.0									-
35   GPZ   5042.50   63.2   73.2   4979.30   4969.30   10.0     36   GPZ   5059.35   82.3   92.3   4977.05   4967.05   10.0     37   GPZ   5039.35   82.3   92.3   4977.05   4967.05   10.0     38   LLZZ   5044.32   126.5   136.5   4917.82   4907.82   10.0     39   LLZZ   5044.06   123.0   133.0   4926.35   4916.35   10.0     40   .LZZ   5044.06   123.0   137.0   4926.35   4915.35   10.0     41   ULZZ   5046.77   92.0   97.0   4954.77   4949.77   5.0     42   ULZZ   5057.33   105.0   115.0   4952.33   4942.33   10.0     43   LLZZ   5057.74   127.0   137.0   4930.74   4920.74   10.0     44   ULZZ   5058.71   106.0   115.0   4952.33   4942.71   10.0     45   ULZZ   5090.11   143.0   15.0   4952.71   4942.71 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>									
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$									
37   UPZ   5091,66   115.0   125.0   4976.66   4966.64   10.0     38   LLPZ   5044.32   126.5   136.5   4917.82   4907.82   10.0     39   LLPZ   5044.06   123.0   133.0   4921.06   4917.82   10.0     40   LLPZ   5043.35   117.0   127.0   4926.35   4916.15   10.0     41   ULPZ   5045.77   92.0   97.0   4954.77   4949.77   5.0     42   ULPZ   5057.33   105.0   115.0   4952.33   4942.33   10.0     43   LLPZ   5057.74   127.0   137.0   4930.74   4920.74   10.0     44   ULPZ   5057.74   127.0   137.0   4930.74   4920.74   10.0     45   ULPZ   5090.11   143.0   153.0   4947.11   4920.74   10.0     46   UPZ   5158.83   180.0   195.0   4947.88   4938.98   10.0     47   UPZ   5155.83   180.0   195.0   4975.83   4960.83									
38     LLFZ     5044.32     126.5     136.5     4917.82     4907.82     10.0       39     LLFZ     5044.06     123.0     133.0     4921.06     4911.06     10.0       40     .LLFZ     5044.35     117.0     127.0     4926.35     4916.35     10.0       41     ULFZ     5046.77     92.0     97.0     4954.77     4949.77     5.0       42     ULFZ     5057.33     105.0     115.0     4952.33     4942.33     10.0       43     LLFZ     5057.74     127.0     137.0     4930.74     4920.74     10.0       43     LLFZ     5057.74     127.0     137.0     4930.74     4920.74     10.0       44     0LFZ     5058.71     106.0     116.0     4952.71     4942.71     10.0       45     ULFZ     5090.11     143.0     153.0     4947.11     4937.11     10.0       45     ULFZ     519.83     190.0     195.0     4975.83     4960.83     15.0 <tr< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr<>									
39     LLPZ     5044.06     123.0     133.0     4921.06     4911.06     10.0       40     .LPZ     5043.35     117.0     127.0     4926.35     4916.35     10.0       41     ULPZ     5046.77     92.0     97.0     4954.77     4949.77     5.0       42     ULPZ     5057.33     105.0     115.0     4930.74     4920.74     10.0       43     LLPZ     5057.74     127.0     137.0     4930.74     4920.74     10.0       44     ULPZ     5057.74     127.0     137.0     4930.74     4920.74     10.0       43     LLPZ     5057.74     127.0     137.0     4930.74     4920.74     10.0       44     ULPZ     5058.71     106.0     116.0     4952.71     4942.71     10.0       45     ULPZ     518.71     106.0     148.0     4938.98     10.0       46     ULPZ     518.83     170.0     180.0     4946.98     4938.98     10.0       47									
40   .LLPZ   5043.35   117.0   127.0   4926.35   4916.35   10.0     41   ULPZ   5046.77   92.0   97.0   4954.77   4949.77   5.0     42   ULPZ   5057.33   105.0   115.0   4952.33   4942.33   10.0     43   LLPZ   5057.74   127.0   137.0   4930.74   4920.74   10.0     44   ULPZ   5058.71   106.0   116.0   4952.71   4942.71   10.0     45   ULPZ   5090.11   143.0   153.0   4947.11   4937.11   10.0     45   ULPZ   518.98   170.0   180.0   4948.98   4938.98   10.0     46   ULPZ   5158.83   180.0   195.0   4975.83   4960.83   15.0     47   UPZ   5168.31   192.0   207.0   4976.31   4961.31   15.0     48   UPZ   5168.31   192.0   207.0   4976.51   4961.51   15.0     50   UPZ   5168.31   192.0   207.0   4976.51   4961.51									-
41   ULFZ   \$046.77   92.0   97.0   4954.77   4949.77   5.0     42   ULFZ   \$057.33   105.0   115.0   4952.33   4942.33   10.0     43   LLFZ   \$057.74   127.0   137.0   4930.74   4920.74   10.0     44   ULFZ   \$058.71   106.0   116.0   4952.71   4942.71   10.0     45   ULFZ   \$090.11   143.0   153.0   4947.11   4937.11   10.0     45   ULFZ   \$118.98   170.0   180.0   4948.98   4938.98   10.0     46   ULFZ   \$118.98   170.0   180.0   4948.98   4938.98   10.0     47   UFZ   \$155.83   180.0   195.0   4975.83   4960.83   15.0     48   UFZ   \$168.31   192.0   207.0   4976.31   4961.31   15.0     49   3rdFZ   \$043.67   137.7   147.7   4905.97   10.0   0     50   UFZ   \$211.51   235.0   250.0   4976.51   4961.51   <									
42   ULPZ   5057.33   105.0   115.0   4952.33   4942.33   10.0     43   LLPZ   5057.74   127.0   137.0   4930.74   4920.74   10.0     44   ULPZ   5058.71   106.0   116.0   4952.71   4942.71   10.0     45   ULPZ   5090.11   143.0   153.0   4947.11   4937.11   10.0     45   ULPZ   518.98   170.0   180.0   4948.98   4938.98   10.0     46   ULPZ   5155.83   180.0   195.0   4975.83   4960.83   15.0     47   UPZ   5155.83   180.0   195.0   4976.31   4961.31   15.0     48   UPZ   5168.31   192.0   207.0   4976.31   4961.31   15.0     48   UPZ   5168.36   7.137.7   147.7   4965.97   10.0   0.0     50   UPZ   5211.51   235.0   250.0   4975.51   4961.51   15.0     51   UPZ   5058.86   75.0   85.0   4983.86   4973.86									
43   LLPZ   5057.74   127.0   137.0   4930.74   4920.74   10.0     44   ULPZ   5058.71   106.0   116.0   4952.71   4942.71   10.0     45   ULPZ   5090.11   143.0   151.0   4947.11   4937.11   10.0     46   ULPZ   518.98   170.0   180.0   4947.11   4937.11   10.0     47   UPZ   5155.83   180.0   195.0   4975.83   4960.83   15.0     48   UPZ   5168.31   192.0   207.0   4976.31   4961.31   15.0     49   3rdPZ   5043.67   137.7   147.7   4965.97   10.0     50   UPZ   5211.51   235.0   250.0   4976.31   4961.51   15.0     50   UPZ   5058.86   75.0   85.0   4983.86   4973.86   10.0     51   UPZ   5058.86   75.0   85.0   4983.86   4973.86   10.0     52   UPZ   5058.86   75.0   85.0   4983.86   4973.86   10.0									
44   ULPZ   5058.71   106.0   116.0   4952.71   4942.71   10.0     45   ULPZ   5090.11   143.0   153.0   4947.11   4937.11   10.0     46   ULPZ   5118.98   170.0   180.0   4948.98   4938.98   10.0     47   UPZ   5155.83   180.0   195.0   4975.83   4960.83   15.0     48   UPZ   5168.31   192.0   207.0   4976.31   4961.31   15.0     49   3rdPZ   5043.67   137.7   147.7   4905.97   4895.97   10.0     50   UPZ   5211.51   235.0   250.0   4976.51   4961.51   15.0     51   UPZ   5058.86   75.0   85.0   4983.86   4973.86   10.0     51   UPZ   5058.86   75.0   85.0   4983.86   4973.86   10.0     52   UPZ   5058.86   75.0   85.0   4983.86   4973.86   10.0     53   UPZ   5058.86   75.0   85.0   4983.86   4973.86									
45   ULFZ   5090.11   143.0   153.0   4947.11   4937.11   10.0     46   ULFZ   5118.98   170.0   180.0   4948.98   4938.98   10.0     47   UFZ   5155.83   190.0   195.0   4975.83   4960.83   15.0     48   UFZ   5168.31   192.0   207.0   4976.31   4961.31   15.0     49   3rdFZ   5043.67   137.7   147.7   4905.97   4895.97   10.0     50   UFZ   5211.51   235.0   230.0   4975.51   4961.51   15.0     51   UFZ   5058.86   75.0   85.0   4983.86   4973.86   10.0     51   UFZ   5156.79   181.8   197.0   4975.01   4959.81   15.2     53   UFZ   5164.24   189.8   204.0   4974.44   4960.24   14.2     (**)   54   UFZ   5158.61   220.0   230.0   4983.61   4903.61   10.0     55   LLFZ   5168.61   220.0   230.0   4981.61   <									
45   ULPZ   \$118.98   170.0   180.0   4948.98   4938.98   10.0     47   UPZ   5155.83   180.0   195.0   4975.83   4960.83   15.0     48   UPZ   5168.31   192.0   207.0   4976.31   4961.31   15.0     49   3rdFZ   5043.67   137.7   147.7   4905.97   4895.97   10.0     50   UFZ   5211.51   235.0   250.0   4976.51   4961.51   15.0     51   UFZ   5058.86   75.0   85.0   4983.86   4973.86   10.0     52   UFZ   5156.79   181.8   197.0   4975.01   4959.81   15.2     53   UFZ   5164.24   189.8   204.0   4974.44   4960.24   14.2     (**)   54   UFZ   5164.61   255.0   265.0   4913.61   4903.61   10.0     55   LLFZ   5164.61   220.0   230.0   4974.64   4965.64   15.0     6   UFZ   5164.61   20.0   230.0   4923.61								-	
47   UFZ   5155.83   180.0   195.0   4975.83   4960.83   15.0     48   UFZ   5168.31   192.0   207.0   4976.31   4961.31   15.0     49   3rdFZ   5043.67   137.7   147.7   4905.97   4895.97   10.0     50   UFZ   5211.51   235.0   250.0   4976.51   4961.51   15.0     51   UFZ   5058.86   75.0   85.0   4983.86   4973.86   10.0     52   UFZ   5156.79   181.8   197.0   4975.01   4959.81   15.2     53   UFZ   5164.24   189.8   204.0   4974.44   4960.24   14.2     (**)   54   UFZ   5158.61   17.0   132.0   4980.64   4965.64   15.0     55   LLFZ   5168.61   220.0   230.0   4913.61   4903.61   10.0     56   UFZ   5168.61   220.0   230.0   4948.61   4933.61   10.0     57   UFZ   5168.61   220.0   230.0   4948.61									
48   UPZ   5168.31   192.0   207.0   4976.31   4961.31   15.0     49   3rdFZ   5043.67   137.7   147.7   4905.97   4895.97   10.0     50   UFZ   5211.51   235.0   250.0   4976.51   4961.51   15.0     51   UFZ   5058.86   75.0   85.0   4983.86   4973.86   10.0     52   UFZ   5156.79   181.8   197.0   4975.01   4959.81   15.2     53   UFZ   5164.24   189.8   204.0   4974.44   4960.24   14.2     (**)   54   UFZ   5097.64   117.0   132.0   4980.64   4965.64   15.0     55   LUFZ   5168.61   255.0   265.0   4913.61   4903.61   10.0     56   UUFZ   5168.61   220.0   230.0   4948.61   4938.61   10.0     57   UFZ   5103.54   126.0   141.0   4977.54   4962.54   15.0									
49   3rdFZ   5043.67   137.7   147.7   4905.97   4895.97   10.0     50   UFZ   5211.51   235.0   250.0   4976.51   4961.51   15.0     51   UFZ   5058.86   75.0   85.0   4983.86   4973.86   10.0     52   UFZ   5156.79   181.8   197.0   4975.01   4959.81   15.2     53   UFZ   5164.24   189.8   204.0   4974.44   4960.24   14.2     (**)   54   UFZ   5097.64   117.0   132.0   4980.64   4965.64   15.0     55   LUFZ   5168.61   255.0   265.0   4913.61   4903.61   10.0     56   UUFZ   5168.61   220.0   230.0   4948.61   4938.61   10.0     57   UFZ   5103.54   126.0   141.0   4977.54   4962.54   15.0									
50     UFZ     5211.51     235.0     250.0     4976.51     4961.51     15.0       51     UFZ     5058.86     75.0     85.0     4983.86     4973.86     10.0       52     UFZ     5156.79     181.8     197.0     4975.01     4955.81     15.2       53     UFZ     5164.24     189.8     204.0     4974.44     4960.24     14.2       (**)     54     UFZ     5097.64     117.0     132.0     4980.64     4965.64     15.0       55     LLFZ     5168.61     255.0     265.0     4913.61     4903.61     10.0       56     ULFZ     5168.61     220.0     230.0     4948.61     4938.61     10.0       57     UFZ     5103.54     126.0     141.0     4977.54     4962.54     15.0			-						
51     OFZ     5058.86     75.0     85.0     4983.86     4973.86     10.0       52     OFZ     5156.79     181.8     197.0     4975.01     4959.81     15.2       53     OFZ     5164.24     189.8     204.0     4974.44     4960.24     14.2       (**)     54     OFZ     5097.64     117.0     132.0     4980.64     4965.64     15.0       55     LLFZ     5168.61     255.0     265.0     4913.61     4903.61     10.0       56     ULFZ     5168.61     220.0     230.0     4948.61     4938.61     10.0       57     ULFZ     5103.54     126.0     141.0     4977.54     4962.54     15.0									
57     0FZ     5156.79     181.8     197.0     4975.01     4959.81     15.2       53     0FZ     5164.24     189.8     204.0     4974.44     4960.24     14.2       (*=)     54     0FZ     5097.64     117.0     132.0     4980.64     4965.64     15.0       55     LLFZ     5168.61     255.0     265.0     4913.61     4903.61     10.0       56     0LFZ     5168.61     220.0     230.0     4948.61     4938.61     10.0       57     0FZ     5103.54     126.0     141.0     4977.54     4962.54     15.0									
53     UPZ     5164.24     189.8     204.0     4974.44     4960.24     14.2       (**)     54     UPZ     5097.64     117.0     132.0     4980.64     4965.64     15.0       55     LLFZ     5168.61     255.0     265.0     4913.61     4903.61     10.0       56     ULFZ     5168.61     220.0     230.0     4948.61     4938.61     10.0       57     UFZ     5103.54     126.0     141.0     4977.54     4962.54     15.0									
(**) 54 072 5097.64 117.0 232.0 4980.64 4965.64 15.0 55 LLFZ 5168.61 255.0 265.0 4913.61 4903.61 10.0 56 0LFZ 5168.61 220.0 230.0 4948.61 4938.61 10.0 57 07Z 5103.54 126.0 141.0 4977.54 4962.54 15.0			072			197-0	4975.01	4959.81	
55     LLFZ     5168.61     255.0     265.0     4913.61     4903.61     10.0       56     ULFZ     5168.61     220.0     230.0     4948.61     4938.61     10.0       57     UFZ     5103.54     126.0     141.0     4977.54     4962.54     15.0			UTZ				4974.44	4960.24	
56 ULTZ 5168.61 220.0 230.0 4948.61 4938.61 10.0 57 UTZ 5103.54 126.0 141.0 4977.54 4962.54 15.0	(**)	54	072	5097,64	117.0	132.0	4980,64	4965.64	
· 57 UTZ 5103.54 126.0 141.0 4977.54 4962.54 15.0		55	LLFZ	5168.51	255.0	265.0	4913.61	4903.61	10.0
		\$6	UL72	\$158.51	220.0	230_0	4948.61	4938.61	10.0
58 UFZ 5158,89 194.0 209.0 4974.89 4959,89 13.0	-	57	422	\$103.54	126.0	141.0	4977.54	4962.54	
		58	UZZ	5158,89	194.0	209.0	4974.89	4959.89	13.0

Table 1 (cont.)

WELL NUMBER	ZONE *	MEASURING POINT ELEVATION	DEPTH TO TOP OF SCREEN (FT.)	DEPTH TO BOTTOM OF SCREEN (FT.)	ÉLEVATION AT TOP OF SCREEN (FT.,MSL)	ELEVATION AT BOTTOM OF SCREEN (FT.,MSL)	Length of Screen (FT.)
59	ULFZ	5059,18	104.5	115.0	4954.58	4944,18	10,5
60	ULFZ	5134.72	185.0	195.0	4949.72	4939.72	10,0
61	UFZ	5133.98	158.0	173.0	4975.88	4950.98	15.0
62	UFZ	5075.00	95.0	110.0	4990.00	4965.00	15.0
63	UFZ	5065.74	83.0	98.D	4932.74	4957.74	15.0
64	VLFZ	5097.84	138.8	149.0	4959.04	4948.84	10.2
PZ-1	UFZ	5142.17	192.7	195.0	4059.47	4944.17	15.3
65	LLFZ	5155.45	260.0	270.0	4895,45	4885,45	10.0
66	LLFZ	5103.03	200.0	210.0	4903.03	4693.03	10.0
67	3rd FZ	5169.21	370.0	380.0	4799.21	4789.21	10.0
68	UFZ	5165.53	194,D	214.0	4971.53	4951.53	20.0
69	LLFZ	5165.46	250.0	270.0	4905.46	4895.45	10.0

Status

Well Mumber

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(\*) UFZ = UPPER FLOW ZONE

ULFZ = UPPER LOWER FLOW ZONE

LLFZ = LOWER LOWER FLOW LONE 3rdPZ = THIRD FLOW ZORE

(\*\*) WELL # 54 IS NORPUNCTIONAL

THE FOLLOWING WELLS HAVE BEEN MODIFIED OR COMPLETELY PLUGGED:

₽ <del>₩-</del> 1	Plugged back to upper flow zone+ -
	Converted to recovery well
P-1	Plugged
1	Plugged
2	Plugged
3	Plugged
4	Plugged
5	Plugged
6	Plugged
8	Plugged
10	Plugged
11	Plogged
12	Plugged back to upper flow zone+
13	Plugged back to upper flow zonet
14	Plugged back to upper flow zone+
15	Plugged back to upper flow zonet
10	Converted to recovery well
23	Converted to recovery well
24	Converted to recovery well
25	Converted to recovery well
26	Converted to recovery well
27	Converted to recovery well
	Converted to recovery well
28	Converted to recovery well
54	Used only for water level measurements

+ ORIGINALLY OPEN TO UFZ, ULFZ, AND LLFZ

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						Sne	artor	Mo	nito	ring	Ree	ulte		-11 <sup></sup>	t	
Sparton Monitoring Results TCE Concentrations																
Date	Year	Qt.	Qtr.	MW-9 UFZ	MW-13 UFZ	MW-14 UFZ	MW-15 UFZ	MW-16 UFZ	MW-19 ULFZ	MW-20		MW-22 UFZ	MW-29 ULFZ	MW-30 ULFZ	MW-31 ULFZ	M
Oct-83			1	21000		12000	1	37000	C							F
Oct-84	1984		3	9600 7300		1 12000	4400	37000								
Jan-86 Apr-86			1 10													┝
Jul-86	1	3	1 12	5000				20000								F
Oct-88 Jan-87						4900		36000 21000				230 170				+-
Apr-87		2	2 15	3600		1800	580	23000	2900	32	1400	270				F.
Jul-87 Oct-87		3				2100		25000 28000	4600	the second second	2100 2000	370 240			<u> </u>	
Jan-88				5500		6200		26000	2900	10	1800	150				
Apr-88		2				5000		25000	5			230				-
Jul-88 Oct-88		3	20			5200 5600	380 250		1800 3600			63 120		·		-
Jan-89	1989		22	4000		3300	180	16000	3200	the second s	The second s	110				F
Feb-89 Mar-89					610 650		210						<u>5.7</u> 5.4	320 320		
Apr-89		2	23	4400		4900	200	14000	3700			150				
Aug-89 Aug-89		3				3000	200	13000	2400	20	460	120				
Nov-89		4	25	2300		2200	260	16000	1500	5	1100	91				
Nov-89	4000	4	-			2100	100	13000	880	17	1000	110		·		-
Jan-90 Jan-90	•	1	26			2100			000	1/	1000					
Apr-90		2	27	2400		1800	160	20000	1000	21	400	130				
Apr-90 Jun-90	<u> </u>	2											7 <b></b>	~~~~		-
Aug-90		3	28	2200		2100	230	19000	850	15	670	140				
Aug-90 Sep-90		3												<b></b>		
Oct-90		Ă	29	1600		1500	140	16000	590	10	850	83				_
Oct-90 Oct-90		4	29	ň		<u> </u>										
Jan-91		1	distant.	1700		1700	110	16000	680	28	910	75				-
Apr-91		2				1400	5		690		400	92		480		
Jun-91 Jul-91		2			330	1100		17000 16000	570 190		500 440	110	<5	180	60	-
Oct-91		4	33	1000		1100		12000	170	+	880	93				
Nov-91 Dec-91		4					· · · · · ·									
Jan-92		1	34	1200		1300		13000	130		680	65				
Apr-92 Jul-92		23				1400	54 49		230		360 390	90 72				
Sep-02		4	37	1000		1100	66	14000	120	30	460	48				
Jan-93	1993					850		13000	57	3	430	51			•	
Apr-93 Jul-93		2		820 730		850 720	1.9 56	12000	110 62	31 7	240 350	55 47				
Oct-93		4	41	680		700	44	13000	45	23	480	41				
Dec-93 Jan-94	1994		-	680 790	330	640 680		13000	<u>39</u> 48		490 380	41	1	47	10	
Apr-94		Ž	43	740		730		11000	81	0.2	280	62				
Jul-94 Oct-94		3		750 750		730 700	<u>52</u> 31		<u>61</u> 47	8 44	210	44				
Oct-94		4	45													
Feb-95 Apr-95	1995	1 2		850 790		690 1000	45	8700	72 92	0.2	270 160	72 100				
Aug-95		3	48	490		470	21	9100	39	11	200	32				-
Oct-95 Jan-96	1000	4	49	650	300	470	15	7400	48		280	34				2
Jan-96 Apr-96	1990	2	50 51	570 710	380	290 420		7600 9700	24 88	1.3	220	46 81	0.9	19	2.7	
Jul-96		3	+ · · ·			300		7400	11	<1	180	43				
			<b>.</b>			L		l		<u> </u>						
				Cluster i Cluster i			Cluster t Cluster t			Cluster #						
				Cluster	#3 = 14,	31,40,4	<b>Cluster</b>	#8 = 51,£	59	Cluster #						
Printed ;	स्तक्र7-केवे.	wiel		Cluster Cluster			Cluster i Cluster i				NOTES				Finge 1 of 4	

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Table 2 (cont.)

and the Constant						Spa	rtor	Mo	nito	ring	Re	sults	)			
											tion					
Date	Year	06.	Q¥.	MW-33	WW-34	UFZ	MW-36 UFZ	MW-37	MW-38	MW-39	MW-40	MW-41 ULFZ	MW-42 ULFZ	MW-43	MW-44 ULFZ	MW-
Oct-83			_					1				1			1	
Oct-84	1984	4				1									]	
	1985		_	<u> </u>			ļ		+	<u> </u>	<u> </u>				<u> </u>	<u> </u>
Jan-86 Apr-86		1 2			<b></b>	+	<b> </b>	ł	<b> </b>	<u>+</u>		<b> </b>			<u> </u>	
Jul-86	<u> </u>	3					ļ	†						~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<b>†</b>	<u>†</u>
Oct-86		4							1		1	1				
Jan-87	1987	1														
Apr-87		23							<b> </b>	<u> </u>	+					
Jul-87 Oct-87		4			<u>+</u>	+			l							
Jan-88	1988	And in case of the local division of the loc	18			1										
Apr-88		2	19													
Jul-88		3									ļ					
Oct-88 Jan-89	4000	4									ļ					
Feb-89	1989	1	22			ļ		ļ								
Mar-89		1	22													
Apr-89		2	23			-										
Aug-89		3	24		<5	<5	7.9	1100								
Aug-89		3	.24		<5	<5	11	1800								
Nov-89		4	25 25						<5	<5	<5	1100	1100	270		
Nov-89 Jan-90	18061	4	26		•				<5	<5	<5	960	1200	160	<5	14
Jan-90	1380	1	26			ł·									<5	14
Apr-90		2	27	F		1		h								
Apr-90		2	27													
Jun-90		2	27													*
Aug-90		3	28													
Aug-90 Sep-90		3	28 28			<u> </u>										
Oct-90		- 4	29													
Oct-90		4	29	·												
Oct-90		4	29													
Jan-91	1991	1	30						-							
Apr-91 Jun-91		2	31	7300	<5	<5	22	2000	<5	~5	<5	620	1000	280	<5	7
Jul-91		3	32	7500				2000					1000	200		
Oct-91		4	33			<5	19	1400					930	440		
Nov-91		4	33													
Dec-91	1002	-4	33													
Jan-92 Apr-92	1997	1	34 35			<5 <5	15	1200					740	260		•
Jul-92		3	36			<5	10	960 800		a			690 640	<u>340</u> 200		
Sep-92		4				<5	8.3	810				510	600	180		
Jan-93	1993	1	38			<1	7	510					680	200		
Apr-93		2	39			<1	4	340					320	130		
Jul-93 Oct-93		3	40 41			<1	25 3					370	620	850	<1	
Dec-93		4	41		<1	<1	3	980	<1	~ <1	<1	350	600 620	160 150	<1	16
Jan-94	1994	1	42			ব	3	860					570	150	<u> </u>	
Apr-94		2	43			<1	2	850					490	120		
Jul-94		3	44			<1	3	370					530	160		
Oct-94 Oct-94		2 3 4 4	45 45			ND	2	940				420	510	110		
Feb-95	1995	-1	46			<5	3	770					340	79		
Apr-95		2	47			<5	3	750					340	08		
Aug-95		2	48				2	750					340	100		
Oct-95		- 4	49				2	750					350	110		
Jan 96	1996	1	50	2000	<0.3	<0.3	1.9	720	<0.3	<0.3	<0,3	290	470	95	<0.3	5
Apr-96 Jul-96		2	51 52		·		<5 2.4	600 560					250	87		
au			22				2.4	200					330	73		

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Table 2 (cont.)

							Spa			nito nce				6			
Date	Year	I	Qtr. #		MW-47 UF2		MW-49 3rd FZ		MW-51 UFZ	MW-52 UFZ		MW-55 LLFZ	MW-50	WW-57	MW-58 UFZ	ULFZ	M
Oct-83					1				1					Ţ			ļ
Oct-84					Ļ,											Ļ	
Jul-85 Jan-86				ļ				<b></b>	<u> </u>	4		<u> </u>	<u> </u>			+	
Jan-86 Apr-86	1966	2	_		<u> </u>		╆	+		<del> </del>	<b>├</b>		<b> </b>	ł	·		
JUI-86		3						·		1		t		1	+	+	<u>+</u>
Oct-86		4			<u> </u>	<b> </b>	<u> </u>	1	1	1	1	1		<u>+</u>			
Jan-87	1987	1	14	1	i					Γ		[	[		1	1	
Apr-87		2						L	ļ					ļ			L
Jul-87		3			· · · · ·	ļ		ļ		I		<b> </b>		ļ			i
Oct-87	1000	4				l						ļ		Ļ		+	
Jan-88 Apr-88	1968		18 19	<b></b>			<b>∤</b>		ļ	l	l				ļ		
00-144				∦					<u>}</u>	<u>∤</u>			<b> </b>		+		
Oct-88		1 Å	21						<u> </u>	f					1	<u> </u>	
Jan-89	1989		21	<b>}</b> −−−−			1	t	t	t		1	Í	1	†	1	
Feb-89		İ	22						1	1				1	1	1	
Mar-89		1							[					<u> </u>		1	
Apr-89		2	23									[					
Aug-89		3												ļ			
Aug-89		3		ļ				I	ļ			ļ	<u> </u>	ļ			
Nov-89		4					l		ļ						ļ	<b> </b>	
Nov-89 Jan-90	1000		-	4200	310	820	<5			<u></u>				<u> </u>		<b> </b>	
Jan-90	1000		26	2300	330	830	<5					~~		<u> </u>	<u> </u>	1	
Apr-90		2		- 2.000			<u>├_~</u> _		8.5				····	t	t	•	
Apr-90		2	27		·····			<1	6.2			_		•	1	t	
Jun-90		2	27		220	820			6.7	<1	<1						
Aug-90		3				600						13	50				
Aug-90		3				1100						9.2	29	1			
Sep-90		3				930						12	98	<1	20		
Oct-90		4	29 29				┟┅╍╍┥									ব্য	<u> </u>
Oct-90 Oct-90		4		<u>  </u>											22	{I	<
Jan-91	1001		designed in the local division of												<u> </u>	<u> </u>	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
Apr-91		2		}f		•										<u> </u>	
Jun-91		2	31	1300	120	410	<5		<5	<5	<5	45	200	<5	29	<5	<
Jul-91		3	32														
Oct-01		4	33	5200		220			<5	<5		74	210		31	<5	<
Nov-01		4	· 33	2600													
Dec-91	1000	4	33	-												_	
Jan-92	1992	1	34	2300		280			11	6.8		96	260		34		
Apr-92		-2	35	960		290			<5	9.8		120	290		37		<
Sep-92				4200		240			<5 <5	14 16		130	290		37 39		~~<
Jan-93	1993	1	38	1200		360			<1		21	190	370		48		
Apr-93		2	39	1200		310			<1		23	110	230		43		<
Jul-93		3		1400		330			<1		33	240	320		62		
Oct-93		4	41	2100		420			1		30	310	430		64		
Dec-93	1001	4	41	1800	93	350	<1		2	<1	32	380	410	<1	74	<1	
Jan-94	1994	1	42 43	2500 2700		350 340			<1		38	370	430		85		
Apr 94 Jul-94		<u>~</u> 3	43	3200	ł	370			0.6 <1		34 43	390 550	370 370		93 110		
Oct-94		4	45	2100		300				<5	40	580	420	-45	97	~	
Oct-94		4	45								38						
Feb-95	1995	1	46	2600		253			<5		21]	580	340		100		
Apr-95		2	47	2400		300			1	1	41	640	370		120		
Aug-95		- 3	_48	3000		250		]	<5		42	680	360	<5	130		
Oct-95	10000	4	49	3300		270			<1		48	130	350	<1	140		
Jan-96 Apr-98	1990	1	50 51	3200 2300	36	350	₹0.3		<0.3	<0.3	100	940	430		270	<0.3	
101-00		2	52	1900		150 130		<5	<5 <1		36 36	790 510	330 240	< <u>1</u> <1	<u>110</u> 130		1
Jul-96																	

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						Spa	rton	Mo	nito	ring	Res	sults	5
										ntra			
Date	Year	Qtr.			MW-62	MW-63	MW-64	MW-65	[MW-66	MW-67	MW-68	MW-69	Comments
Ocl-83	1983	4	#	UFZ	UFZ	UFZ	ULFZ	LLFZ	<u>LLFZ</u>	3rdFZ	UFZ	LLFZ	
Oct-84	1984	4				1	1						
Jul-85		3				<u> </u>							
Jan-96		1	10		I	ļ			l		·	ļ	
Apr-86 Jul-86		23		ļ		· · · · ·							
Oct-86		- Ă				ł							
Jary 87	1987	1	14										1
Apr-87		2											
Jul-87		3			· · · · · · · · · · · · · · · · · · ·								·
Oct-87 Jan-88	1088												
Apr-88	1900	2											
Jul-88		3	20		~								
Oct-88		4											
Jan-89	1989	1									•		
Feb-89 Mar-89		1	22 22						<u> </u>				
Apr-89			23									·	
Aug-89		3	24										
Aug-89		3	-24										
Nov-89	-	4	25										#42843 actual 12-12-09
Nov-89 Jan-90	4000	4	25										#42843 actual 12-21-89 #49 - actual 01-25-90
Jan-90	1990	1	26 26										#49 - actual 01-25-90
Apr-90		2	27										1-13 - BEIGHI VI-31-80
Apr-B0		2	27	····									
Jun-90		2	27								· · · · · · · · · · · · · · · · · · ·	~	#51 - actual 05-07-90
Aug-90		3	28										
Aug-90		3	28										
Sep-90 Oct-90		3	28 29	<1	<5	<1	<5						
Oct-90		- 4	29	<5	2.2	<5	<1						
Oct-90		4	29	<5	<5	<5	<5						
Jan-91	1991	1	30										
Apr-91		2	31										
Jun-91 Jul-91		23	31 32	<5	<5	<5	<5						EPA split sample
00-91			<u>33</u>		<5							•	
Nov-91		4	33										
Dec-91		4	33	,									
Jan-92	1992	1	34		<5								
Apr-92		2	<u>35</u> 36		<5								
Jul-92 Sep-92	+	- J - 4	30		<5 <5								
Jan-93	1993	-1	38		2								
Apr-93		2	39		2								
Jul-93	-	3	40	490	3								
Oct-93			41	500	3								#61 - actual 09-03-93
Dec-93 Jan-94	1004	-4	41	610 530	3	<1	<1						EPA split sample
Apr-94	1994	1	42		2 2								#51 = J value
Jul-94		3	44	800	3								#31 - 3 Value
Oct-94		4	45	870	2		10						#62,36 = J value, EPA split samp
Oct-94	10	4	45										#53 duplicate sample
Feb-95	1995	1	46 47	960 1400	2	-	11						#36 & 62 = J values
Apr-95 Aug-95		2	4/ 4B	1700	2		18 17						#36, 51 & 62 = J values #36 & 62 = J values
Oct-95		4	49	2000	2		8						
Jan-96	1996	1	50	1900	1.8	<0.3	15		+				EPA split sample
Apr-96		2	51	1100	<5		25						EPA split sample
Jul-96		3	52	780	1.7		32	1.5	<1	1	<1	<1	#66 sampled 6/27/96 & 7/18/96

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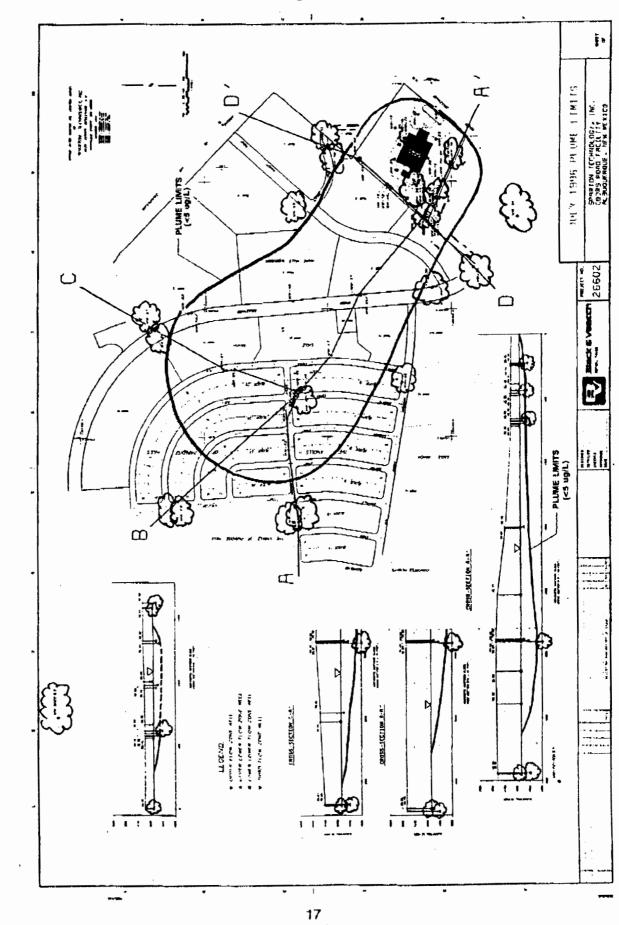
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Figure 5



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No.

- Transverse UFZ section along west side of Sparton facility (MW-35, MW-3. 14, MW-21, MW-51) shows range from non-detect to 420 µg/l to nondetect.
- ULFZ section along Irving Boulevard (wells MW-44, MW-45, MW-46, MW-4. 64) shows range from non-detect to 3200 µg/l to 32 µg/l.

Plume delineation is also confirmed by the decreasing TCE concentration with depth at all but one of the 13 vertical cluster wells. In the one increasing cluster consisting of MW-15. MW-41 and MW-32 the bottom LLFZ well MW-32 is not as deep as bottom wells in adjacent clusters. The terminology decreasing with depth means that the bottom well in a vertical cluster shows lower concentration (usually non-detect) than the other wells in the cluster.

Monitor well installation and sampling began in 1983. Through continued well installation and sampling through July 1996, it has been possible to track the development or evolution of the plume to its present form. The shape, both horizontally and vertically, is shown on previous Figure 5.

In the early stages of monitoring, both onsite and near offsite investigation utilized a high density (close-spaced) network of monitoring wells to characterize the plume and subsurface conditions. However, as confidence in the understanding of the plume and subsurface conditions increased, continuing investigations began using greater well spacings to primarily confirm the understanding and to fill, if needed, any data gaps. As the investigations moved further offsite, no anomalous conditions were encountered which would have required more intensive study. The most recent investigation (consisting of the five wells installed in summer 1996) successfully addressed concerns and questions raised since the last previous intrusive investigation in 1990. The number and locations of current non-detect wells, as shown on Figure 5, are more than adequate to define the plume limits. Further, the number and distribution of wells inside the plume provides excellent areal and vertical definition of concentration.

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Rate of Migration. The TCE plume is migrating in a west-northwest direction at a current rate of less than 100 feet/year. The rate of migration and direction is consistent with the site-specific hydrogeologic characterization. This consistency was expected. Groundwater flow rates are low and relatively uniform based on hydraulic gradient information shown on previous Figure 3. The dissolved, aqueous phase of TCE is relatively mobile and should travel at the same rate (and in the same direction) as groundwater flow. As previously noted, Dr. John Hawley has opined that the TCE plume definition provides an excellent tracer to show groundwater flow rate and direction.

The rate of plume migration can be verified from a consensus of independent analyses:

- 1. Dividing the horizontal downgradient length of the plume (2,800 feet) by the estimated age of the release (30 years) provides an average migration rate of approximately 100 feet/year.
- 2. The prevailing site-specific groundwater flow rate is less than 100 feet/year using site-specific hydraulic gradients obtained from site monitoring wells and site-specific hydraulic conductivity values. Note that the site-specific parameters (and groundwater flow rate) are remarkably consistent with regional hydrogeologic characterization and modelling.
- 3. By comparing TCE plume extent defined by June 1991 sampling with the current plume extent (July 1996), a migration rate of less than 100 feet/year can be clearly demonstrated.

Contaminant Concentrations in Groundwater. Monitoring wells have been sampled since 1983. Continued installation of wells and sampling has determined that the primary constituent of concern is TCE (1992 RFI Report). TCA is also present at approximately one third of the TCE concentration. DCE and DMA are found less frequently. Of the 49 wells sampled in July 1996, 26 had TCE concentrations above 5 µg/l. Maximum TCE concentration was observed in MW-16, a shallow onsite well near the original source area. Highest offsite TCE concentrations were observed in

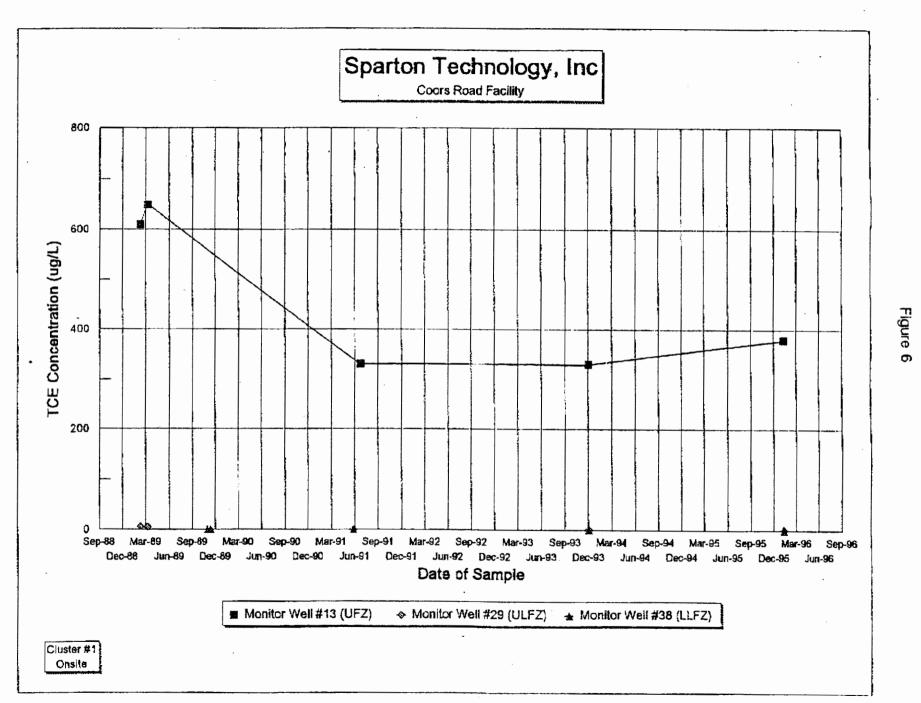
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wells MW-46 and MW-61 in the plume interior. TCE concentration data is given in previous Table 1. Well locations can be obtained from previous Figures 4 and 5.

Plume concentration is decreasing at a much faster rate than that resulting from expansion of the plume. This concentration decrease is the result of previous source material removal, the ongoing, onsite groundwater recovery and treatment implemented in December 1988, and natural attenuation processes. With respect to the TCE concentration data given in previous Table 4, the following trends are readily apparent from the 43 wells with extended time histories:

- 1. Of the 22 UFZ wells, 5 offsite wells (MW-34, MW-35, MW-57, MW-63, MW-62) have non-detection histories. Of the remaining 17 wells, only 3 offsite wells (MW-53, MW-58, MW-61) have increasing concentration histories. The remaining 14 wells (including all on-site UFZ wells) all show decreasing concentration histories.
- 2. Of the 13 ULFZ wells, 2 off-site wells (MW-44, MW-59) have non-detection histories. Three off-site wells (MW-56, MW-60, MW-64) have increasing concentration histories. A single well (MW-46) has an erratic history. The remaining 7 wells (including all on-site ULFZ wells) show decreasing concentration histories.
- З. Of the 7 LLFZ wells, 3 on-site wells (MW-38, MW-39, and MW-40) have non-detection histories. Only a single off-site well (MW-55) shows an increasing concentration history. The remaining 3 wells have decreasing concentration histories.
- 4. There is only a single on-site TFZ well (MW-49) and this well has a nondetection history

The TCE concentration database also shows that of the 13 vertical well clusters shown on previous Figures 4 and 5, only a single well cluster (cluster No. 4 consisting of MW-15, MW-41, and MW-32) shows increasing concentration with depth; however all wells in this cluster have decreasing concentration time histories. Increase in concentration with depth means that the bottom well in a vertical cluster shows higher concentration than the other wells in the cluster. Time-history plots of the 10 vertical clusters with extended time history data are shown on Figures 6 through 15.



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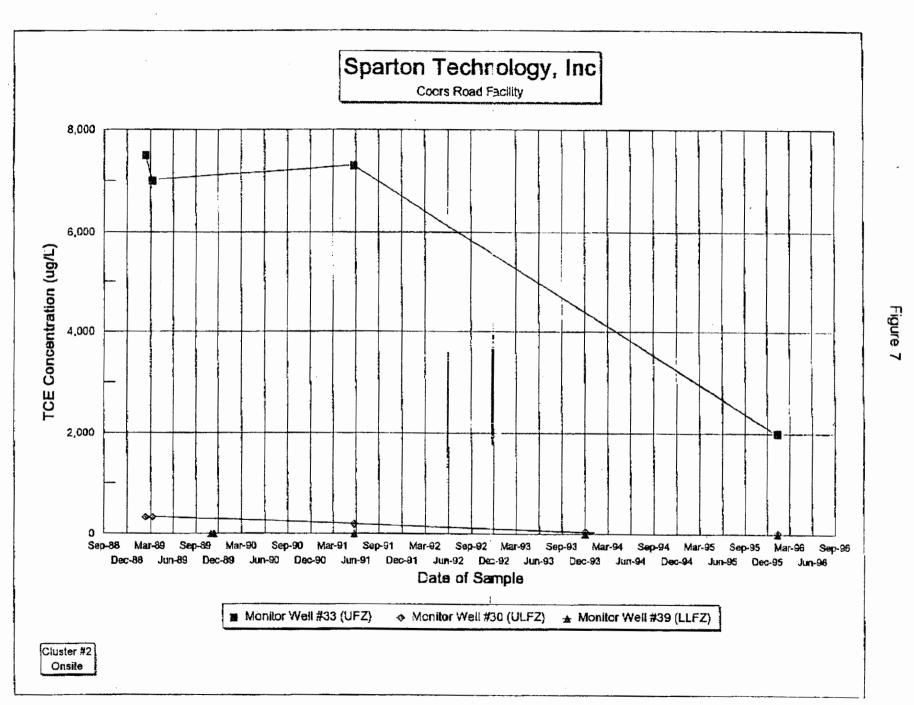
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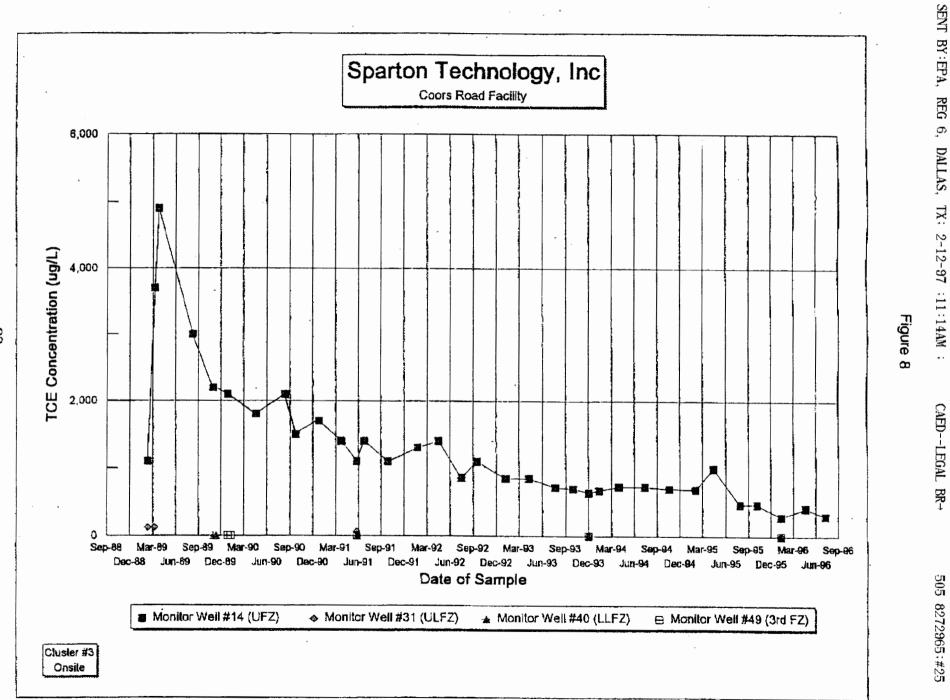
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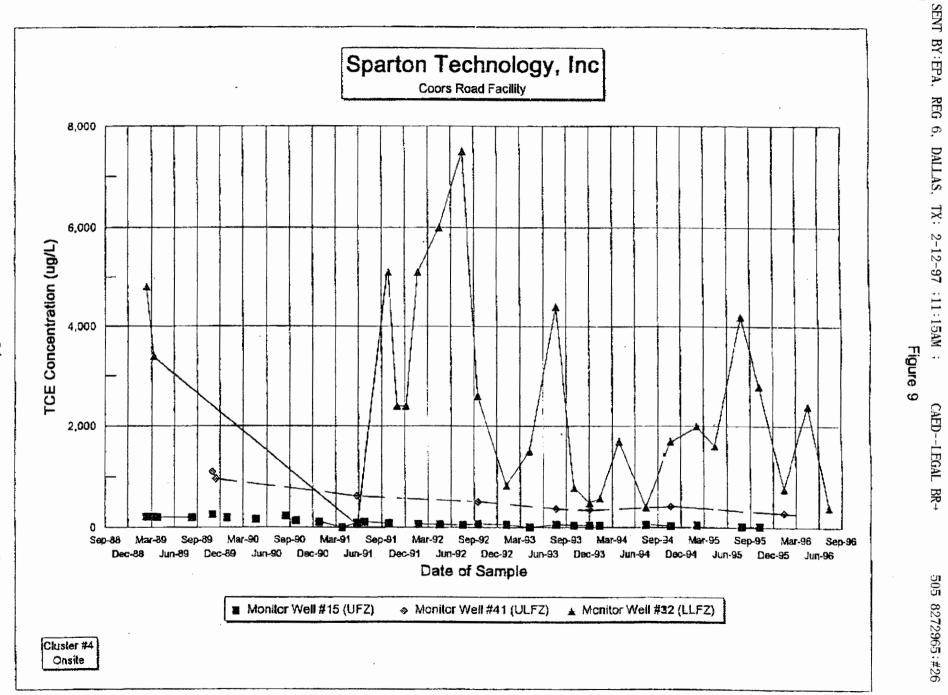
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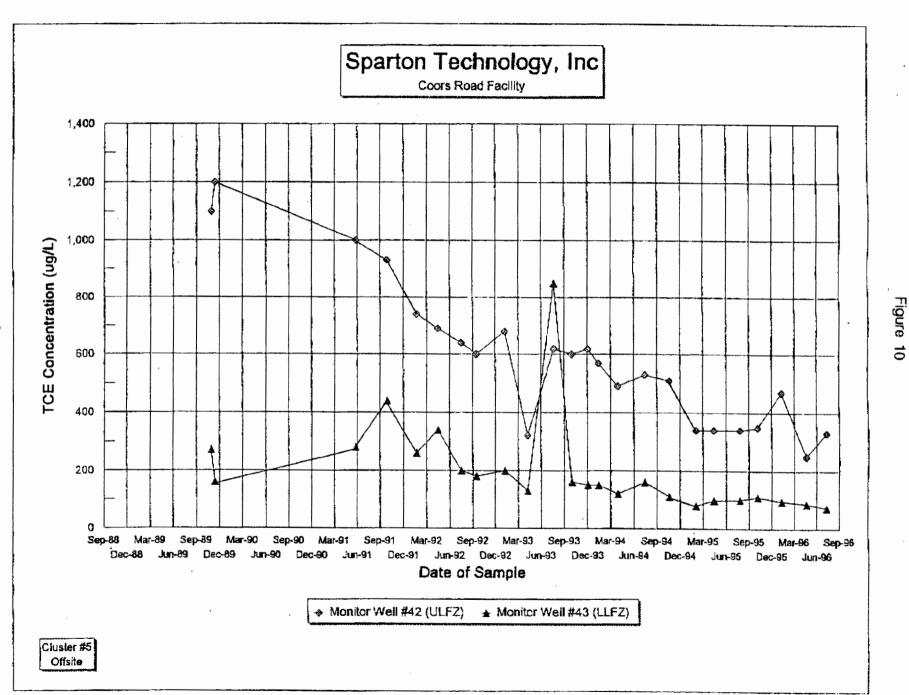
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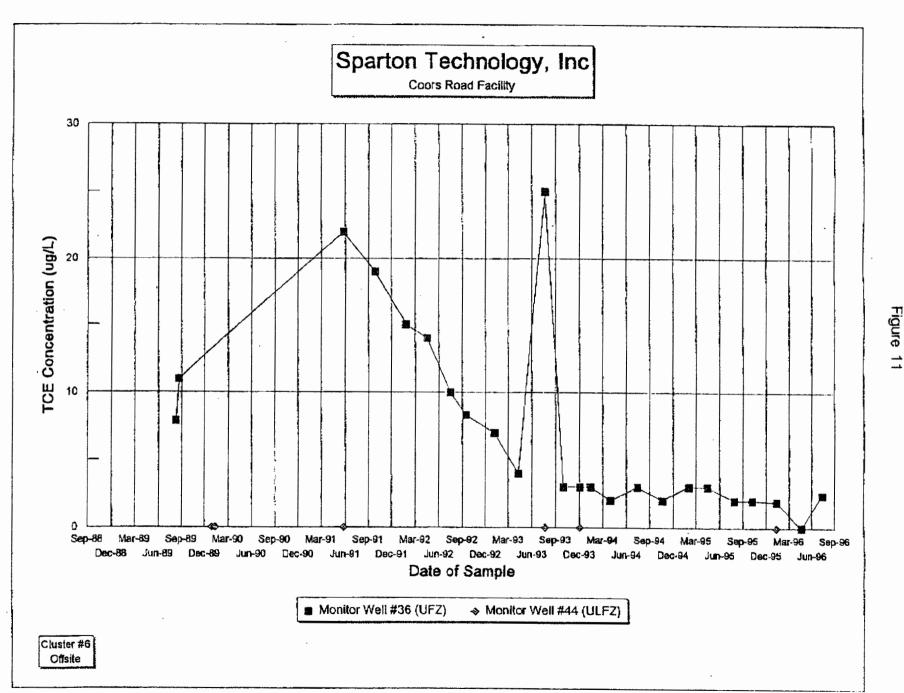
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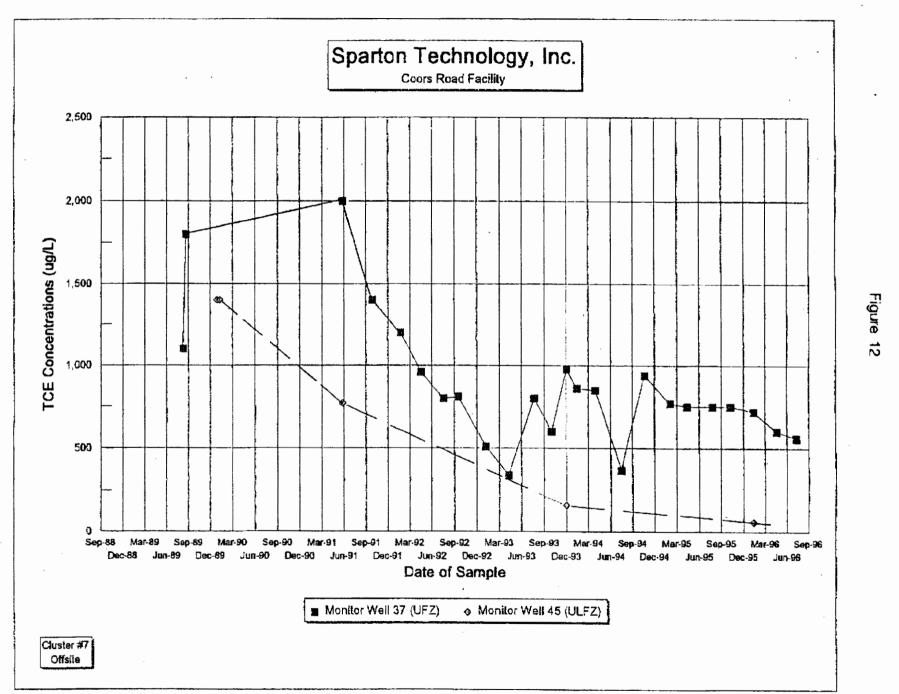
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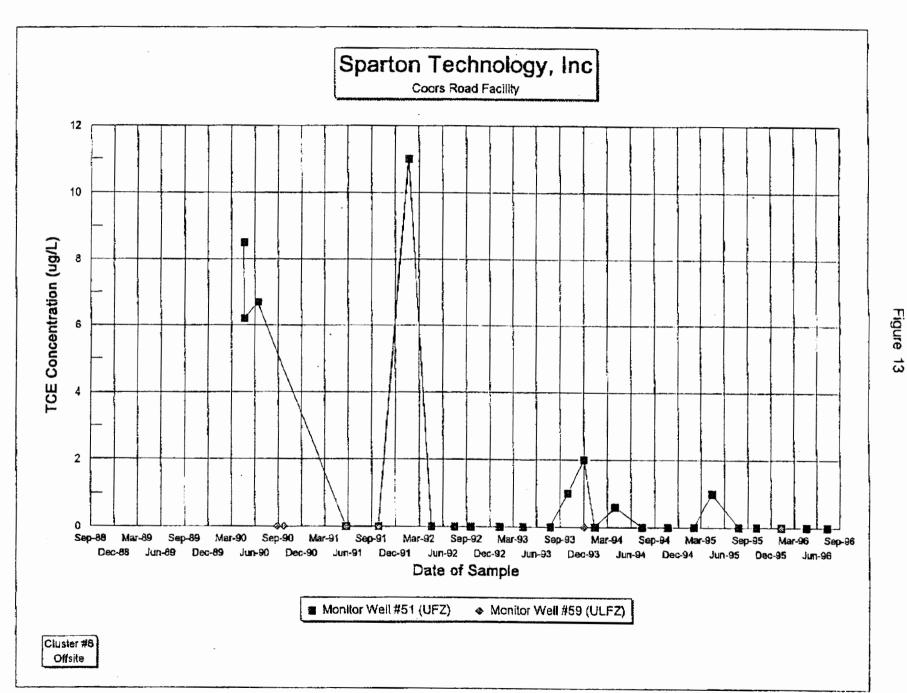
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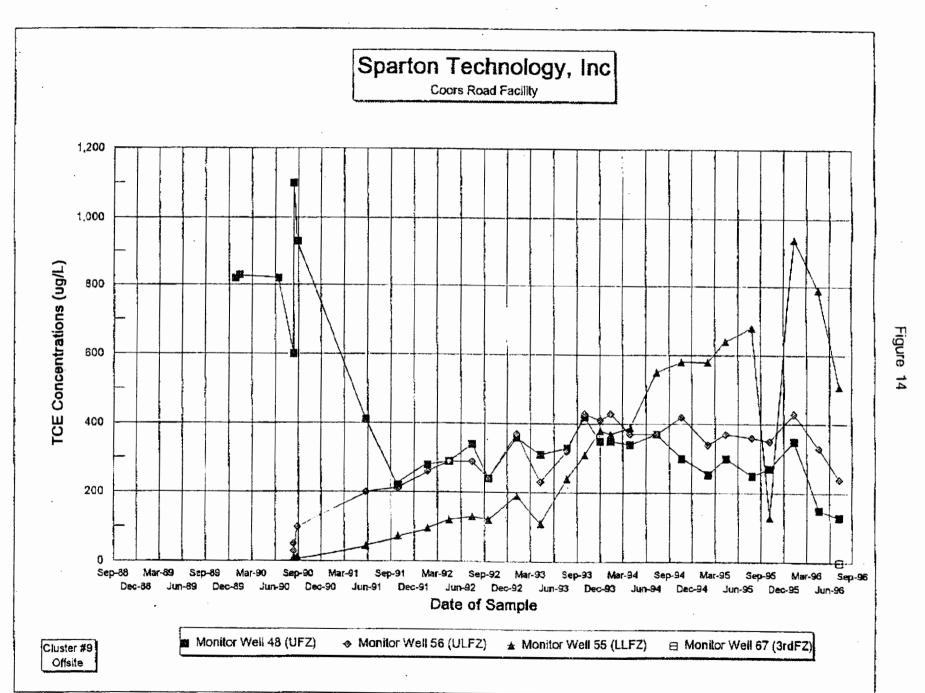
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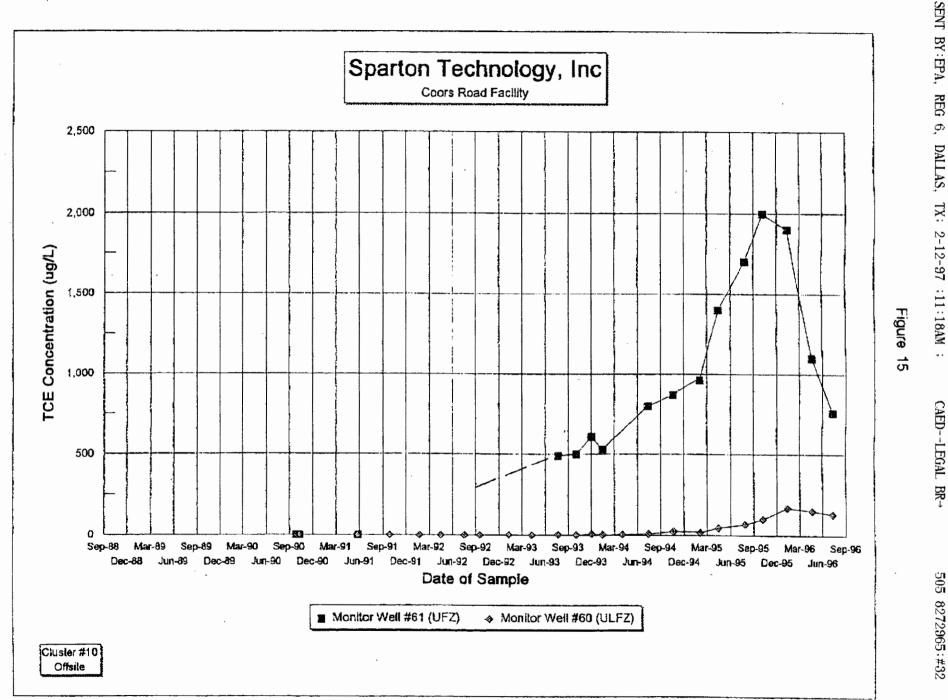
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Decrease in plume concentration is also demonstrated by mapping and contouring of specific volatile organic constituent (VOC) analytical results obtained from a series of surface soil-gas surveys conducted in 1984, 1987, and 1991. Reports detailing each survey are included in the 1992 RFI Report attachments. Survey information is also summarized in the 1996 CMS Report. A comparison of the plotted results shows a significantly progressive decrease in surface soil-gas VOC concentrations including TCE and TCA.

Comparison of soil gas concentrations indicates a fifty-fold decrease in TCE and thirtyfold decrease in TCA concentration in the period 1984 to 1991. In the 1987 and 1991 surveys, TCE and TCA were detected over approximately the same area; however, TCE concentration dropped almost an order of magnitude and TCA concentration dropped 30 to 50 percent.

<u>Need for Additional Contaminant Characterization Study</u>. Additional site investigation beyond continued groundwater monitoring would only confirm current characterization of the plume. Additional investigation will not fundamentally change understanding or definition of the plume relative to assessing risk/threat or remedial design.

Continued monitoring consisting of semi-annual to annual monitoring of selected, representative wells for VOC is more than adequate based on the following:

- 1) Plume limits and direction and rate of movement are defined and understood.
- Plume poses no risk/threat and there are no significant exposure pathways/potential receptors.
- 3) There is an adequate network of groundwater wells around and under (as well as inside) the plume particularly near the leading edge.
- 4) There is an extended history of quarterly results since 1992 and slightly less frequent results dating back into the 1980's as given in previous Table 2.

- Specific VOC (TCE, TCA, DCE, DMA) are constituents of concern for plume definition and risk/threat assessment. Any degradation products will also be VOC.
- 6) Standard groundwater monitoring practice is to decrease monitoring frequency, decrease number of wells sampled, and to limit analyses to constituents of concern as plume (and risk/threat) becomes defined and understood.

### RISK ASSESSMENT

The defined contaminant plume poses no risk or threat to human health. Contaminant concentrations within the plume exceed drinking water standards; however, there is no foreseeable exposure pathway to current (and future planned) drinking water use from the aquifer in the impacted area.

Potential Receptors/Exposure Pathways. The nearest potential receptor/ exposure pathway is the New Mexico Utilities (NMU) municipal supply well some 2.1 miles downgradient from the leading edge of the plume. In addition to the horizontal and vertical separation of the NMU well intake from the plume, modelling conducted in 1996 showed that the plume's continued migration would not affect drinking water quality at the NMU well. The model was intended to represent a "worst-case" relative to risk posed to the NMU well. Model used the high range of hydraulic conductivity, low range of effective porosity, and assumed the site-specific hydraulic gradient extended all the way to the NMU well. Further, it was assumed that no retardation or degradation of TCE was occurring. The model was calibrated to the plume limits (and age) given in the 1992 RFI Report and then run for elapsed times up to several hundred years. The model was never intended to be an exact simulation, but rather was intended to show the non-impact to the NMU well under conservative modelling.

In concern No. 13 of the Technical Review of the CMS Report dated June 20, 1996, EPA was critical of the groundwater modelling and related conclusions without making any effort to understand the assumptions, input parameters, and calibration efforts. EPA also apparently failed to review requested additional supplemental data on the model furnished by Sparton on June 3, 1996.

The model was run using site-specific hydraulic gradient and hydraulic conductivity values included in both the RFI and CMS Reports. Although challenged by EPA, these parameters are remarkably consistent with regional characterization. The model was then calibrated to the RFI Report plume limits by varying longitudinal and transverse dispersivity values to obtain a good match to plume shape. Vertical matching was also checked. In spite of EPA's erroneous assertion, vertical dispersivity was constant at 0.01 which calculates to approximately 0.2 to 2 percent of the calibrated horizontal values. This value for vertical dispersivity is very close to the value EPA claims should have been used in the absence of site-specific data. EPA further challenged Sparton's decision to model the plume migration toward the nearest potential receptor -- the NMU municipal supply well some 2.1 miles distant.

In spite of EPA's strenuous criticism, the calibrated model appears to match the plume shape and rate of migration very well. Predictions based on that model were readily confirmed by the additional groundwater monitoring wells installed in summer 1996.

Threat. Concentrations of TCE, TCA, DCE, and DMA within the plume exceed drinking water standards; however, due to the lack of any realistic exposure pathways and/or potential receptors, the plume poses no current (or reasonably foreseeable) risk/threat to human health. The impacted ground water is not used by any water system and does not pose an ingestion risk to human health. In addition, homes located over the plume are not at risk from soil gas emanating from the plume. Repeated surface soil gas surveys did not detect any VOC in or near the residential area at a detection limit of 0.00022 ppm,. Further, deep soil gas surveys conducted at the top of the saturated zone and reported in the CMS Report, did not detect any significant (<1 ppm,) VOC concentration offsite. Thus, there is no risk by inhalation.

### **AQUIFER RESTORATION**

Subset

Restoration is defined as the removal of contaminants to achieve drinking water standards. It is very doubtful that the impacted aguifer can be restored by any "Technically Practicable" methodology(ies) in any reasonable time frame. This conclusion is based on the following site-specific information:

- 1. The heterogeneous and anisotropic nature of the subsurface will not allow simplistic "broad brush" solutions. "Real world" solutions will have to deal with discrete, isolated contaminant concentrations in attaining restoration.
- Restoration will require removal of both dissolved phase contamination from groundwater and sorbed-phase (residual DNAPL) contamination from saturated fine-grained clays and silts. Sorbed-phase (residual DNAPL) removal will require long-term activity.

Sorbed-phase contamination is the result of constituents being adsorbed onto or bound up by capillary forces within the soil pore structure. Sorption of constituents such as TCE is enhanced by the presence of fine-grained silts and clays and/or organic material. It has been reported by Piwani & Keeley (EPA, 1990) that "a few percent of silts and clays can result in a substantial increase in the sorptive behavior of the aquifer material". These silts and clays are the sorptive sites to contaminants in groundwater moving through the subsurface matrix. Increasing percentages of silts and clays will result in significant sorbed-phase contamination.

Both regional characterization and site-specific investigation show that silts and clays are significantly present and heterogeneously and anisotropically distributed throughout the aquifer. These silts and clays not only restrict vertical migration, but also readily adsorb contaminants from the ground water.

John Hawley summarized properties for the lithofacies (sedimentary geologic units) that make up the Albuquerque Basin (USGS, 1993). Hawley indicates that the ratio of sand plus gravel to silt plus clay will range from a high in excess of two to a low of less than 0.5 for the typical geologic materials in the subsurface. Converted to a percent, these ratios would range from less than 30 percent to over 70 percent silt and clay. A review of boring logs from deeper well installations (LLFZ and TFZ wells) at the Sparton facility indicates that approximately 40 percent of the saturated depth interval is comprised of clay, clayey, or silty stratigraphic units. The remaining units also contain clay/silt seams and lenses; however, the use

of bentonite as a drilling fluid additive makes identification of minor silt/clay very difficult. Actual amount of silt/clay is estimated in the 20 percent range. Recent investigation north of the Calabacillas Arroyo (USBR, 1996) showed that, in the upper 300 feet of the saturated zone: silt/clay was present in 45 of the 60 five-foot logged intervals; silt/clay content ranged from 0 to 85 percent; and average clay content was approximately 15 percent over the total 300 feet. However, the USBR indicated that drilling fluid precluded a complete evaluation of silt/clay fraction.

- 3. Hydraulic conductivity and groundwater flow rates are low. As a result, groundwater extraction and treatment will require a very long time frame because of the extremely large volume of water to be treated and the rate at which the water can be removed by wells.
- 4. The plume is relatively large in horizontal extent due to migration from a long-duration release; however, the plume is relatively thin (in depth) due to the significant vertical anisotropy. The plume dimensions and contaminant distributions will not allow efficient, high-rate groundwater extraction. Highest TCE concentrations are found near the top of the aquifer. Large drawdowns associated with high pumping rates will pull contamination down into lower portions of the aquifer. High pumping rates will also result in more water being removed from the zones with higher hydraulic conductivities (and probably from areas outside the plume) with little effect on either dissolved-phase or sorbed-phase contamination in the less water-transmissive zones. Aggressive pumping will thus result in the removal and treatment of very large volumes of relatively uncontaminated water without achieving significant remediation.
- 5. Attempts to restore the aquifer will require numerous wells pumping at low rates because of the plume size, drawdown limitations, pumping rate limitations, and resultant influence limitations. Because of the time requirements resulting from pumping rate limitations and the difficulty of removal of sorbed-phase contamination, attempts at restoration will be extremely inefficient.

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- 6. The plume is located under a developing residential area. There will be little room for numerous recovery wells. In addition, bringing large quantities of contaminated water to the surface at numerous locations will greatly increase risk/threat to human health.
- 7. EPA Region 6 and NMED have been unable to provide any successful case-history documentation to support restoration under similar conditions/contaminants.

Site characteristics and contamination were also analyzed in the context of EPA's <u>Guidance for Evaluating the Technical Impracticability of Groundwater Restoration</u> (EPA, 1993). Procedures in this guidance lead to the conclusion that aquifer restoration is "Technically Impracticable." Application of the guidance procedures is detailed in both text and table form in the 1996 CMS.Report.

In their Technical Review of the CMS Report dated June 20, 1996, EPA questioned technical impracticability in concern No. 11. EPA appears to differentiate between dissolved-phase and residual-phase VOC (referred to as "entrained DNAPL" in the concern). EPA agrees that entrained DNAPL would prevent practicable restoration, but argues that entrained DNAPL is found only near the source. It is interesting to note that EPA quotes out of context its own technical guidance (EPA, 1993) page 8, and seems to misuse a second quote from page 12 of the guidance. In light of the numerous studies and case histories reported in the literature, and recognizing the conditions at the Sparton facility, it is surprising that EPA does not believe that sorbed-phase VOC or residual DNAPL is not present throughout the plume. Further, EPA seems unwilling to acknowledge the difficulty of residual DNAPL remediation.

The infeasibility of aquifer restoration at this site is further confirmed by the 24 case histories contained in <u>Evaluation of Ground-Water Extraction Remedies</u>: <u>Phase II</u> (EPA, 1992). This report was used by EPA as a "report card" in response to Congressional inquiry. The report was intended to be a summary of the state-of-

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practice for groundwater remediation. The following summary of the reported case histories is extremely relevant to the Sparton facility:

- 1. Contamination 12 of the 24 sites had TCE contamination; 19 of the 24 sites had chlorinated solvent contamination.
- Geology all 12 of the TCE contaminated sites had fluvial clay, silt, sand, and gravel geology; 18 of the 19 chlorinated solvent sites had same geology.
- 3. Extent of Plume the horizontal extent of the plumes was <u>much</u>, <u>much</u> larger than the vertical depth or thickness; the 12 TCE sites ranged from 9 to 760 acres in sizes with depths ranging from 20 to 250 feet; the 19 chlorinated sites ranged from 0.7 to 7,600 acres with depths from 20 to 250 feet.
- Regulatory Program the TCE sites included three RCRA, four Superfund, and five state; the chlorinated sites were three RCRA, six Superfund, and 10 state.
- 5. Containment containment was achieved at eight of the 12 TCE sites; containment was achieved at 13 of the 19 chlorinated solvent sites.
- 6. Restoration restoration was not being achieved, nor had been achieved, at any of the 24 sites.

To-date, EPA has not provided any meaningful case-history data to support the feasibility of restoration. In fact, EPA's Office of Emergency and Remedial Response (OERR) is currently involved in the evaluation of containment as an alternative to restoration because of EPA's dismal experience with restoration and resultant Congressional and technical pressure.

Technical impracticability of restoration at Sparton's site is also confirmed by the additional case history information contained in <u>Alternatives for Groundwater Cleanup</u> (National Research Council, 1994). The above discussions and references are not

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intended to show that groundwater extraction or "pump and treat" is bad; but rather to show that extraction is more appropriate for containment and contaminant reduction as contrasted to restoration.

Although aquifer restoration is technically impracticable, aquifer remediation is realistic and practicable. Sparton's currently proposed remediation activities will produce comparable results to EPA's proposed Alternative 4 over the same 30-year time frame at substantially less cost. Sparton capital costs are approximately \$0.5 million, operation and maintenance costs are approximately \$0.2 million/year. EPA's capital cost is approximately \$2.5 to \$3.1 million with an operations and maintenance cost of approximately \$0.85 to \$3.6 million annually, depending on extent of water treatment. Costs for additional extraction wells were not quantified in the EPA Final Decision (EPA, 1996); however, additional extraction wells were discussed in the context of final-phase restoration. Each additional extraction well (200 gpm nominal pumping), together with its water treatment and reinjection requirements, would have capital costs in the range of \$0.58M to \$0.77M and annual O&M of \$0.2M to \$1.2M, depending on level of treatment.

Sparton's most recent proposed remediation would provide for containment of the leading edge of the plume. This containment would control further plume migration and ultimately capture existing contamination moving downgradient in offsite areas of the plume. Sparton's containment proposal was conditioned to the economical treatment and disposal of extracted groundwater.

In the 1996 CMS Report, Sparton has also proposed expansion of the existing onsite groundwater extraction system to enhance both onsite containment and removal of source material from areas with elevated contaminant concentration. Over eight years of successful operation of this system demonstrate its feasibility.

In their Final Decision Document, EPA provided erroneous and misleading depictions of capture zones for the existing onsite recovery well system. These capture zones are significantly different from, and much smaller than, capture zones and/or radius of influence given in Sparton's Effectiveness Report and in EPA's previous Statement of Basis. In the Final Decision, EPA decided to ignore demonstrations of the actual pumping radius of influence obtained from multiple, multi-well pumping tests :

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conducted on several of the recovery wells. These demonstrations were used to confirm Sparton's calculations for all the recovery wells. EPA elaborated on their calculations under concern No. 1 of their June 20, 1996, Technical Review of the Effectiveness Report. Their comments reflect a basic misunderstanding of the Hyorslev methodology to require "an instantaneous change in the water level" when, in fact, Hvorslev methodology can be applied (and often is) to constant rate or equilibrium conditions (USACOE, 1951). Secondly, EPA averaged well-locationspecific hydraulic conductivities ranging two orders of magnitude and hydraulic gradients ranging over an order of magnitude to obtain single values for calculations at all well locations. Such an approach ignores the significant heterogeneity and anisotropy observed and documented on site. EPA also chose to ignore actual field demonstrations of capture determined from long-duration, multiple-well pump tests included in Appendix 2 of Sparton's Effectiveness Report. For example, for two wells in the original source area, MW-24 and MW-25, EPA calculated maximum capture zone widths of 8.88 and 16.00 feet respectively, yet actual pump test results showed that pumping of either MW-24 or MW-25 impacted the drawdown in the other well over a horizontal distance of 32.82 feet. This demonstration would indicate capture zone widths are at least 66 feet wide at the wells and would be somewhat larger. upgradient. Obviously, inter-well comparisons of influence obtained under actual field conditions are far superior to any theoretical calculations.

In the 1996 CMS Report, Sparton has also proposed installation of a soil vapor extraction (SVE) system to remove source material from the unsaturated zone in the vicinity of the original contamination source area.

Based on the current rate of plume migration, it will take 25 to 30 years for the majority of contamination to be captured by the leading edge containment; however, natural attenuation including biotic and abiotic processes will be taking place based on site observations to date and recent New Mexico Water Resources Research Institute studies in the Albuquerque Basin (NMWRRI, 1992).

### **SUMMARY**

- Subsurface conditions and plume characterization are more than adequately defined and understood; plume behavior is predictable.
- Potential receptor/exposure pathways are identified and there is no risk/threat to human health.
- There is more than sufficient information to assess risk/threat and/or to design any additional remediation; further study or investigation is not needed.
- Sparton's proposed remediation will accomplish the same objectives as EPA's proposal in the same time-frame at significantly less cost.

I state, under penalty of perjury, that the foregoing is true and correct.

Executed on February 4, 1997.

Black & Veatch

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Pierce L. Chandler, Jr. Project Manager

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Attachments:

Curriculum Vitae - Pierce Chandler Bibliography